

Lecture 05

Hydration

- a) Reaction of cement clinker
- b) Hydration modelling with GEMS

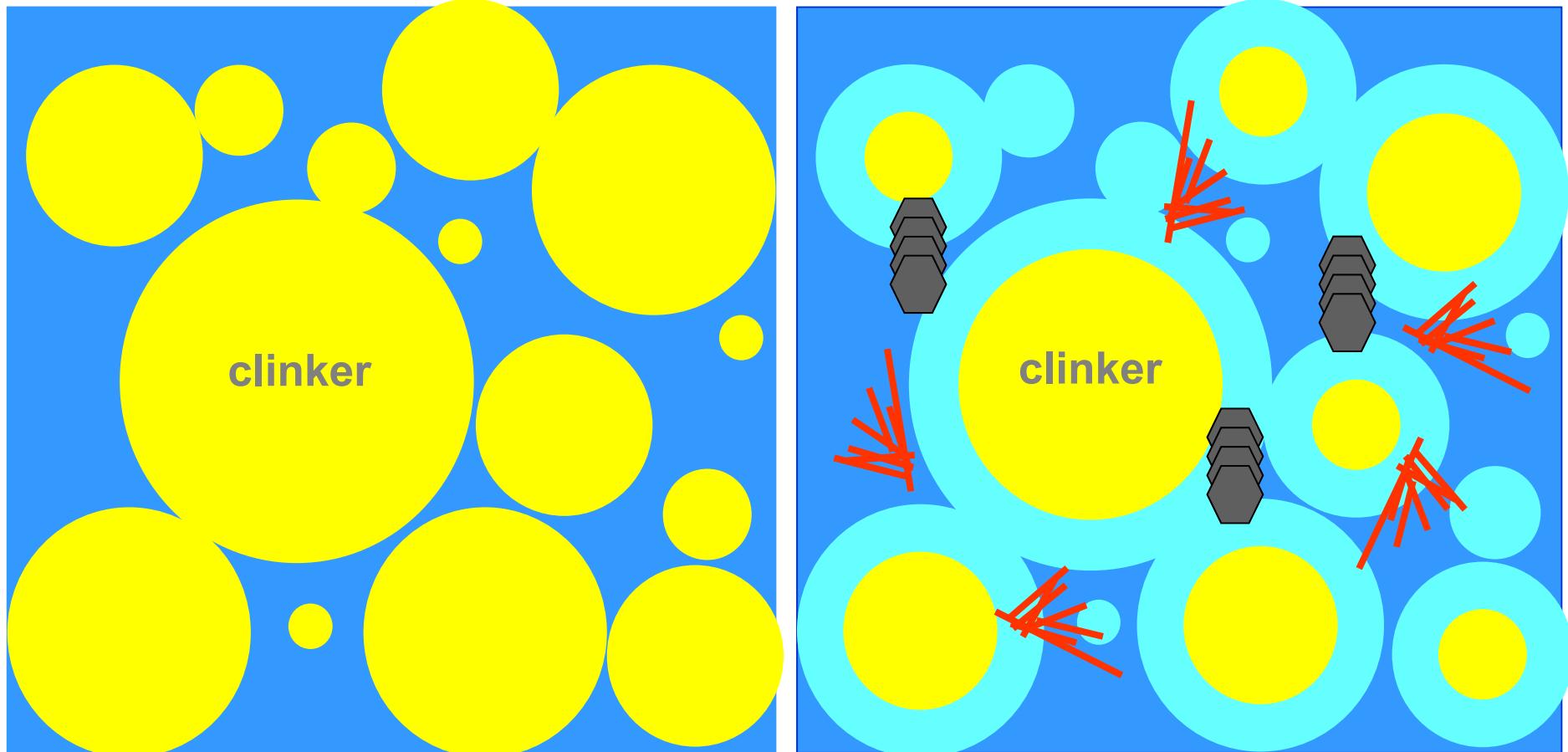
Barbara Lothenbach
Frank Winnefeld
Bin Ma
Zhenguo Shi



Software development/fitting
tools/kinetic:
Dmitrii Kulik
Dan Miron



Hydration



● C-S-H ● Portlandite ↗ Ettringite

Modeling: Dissolution

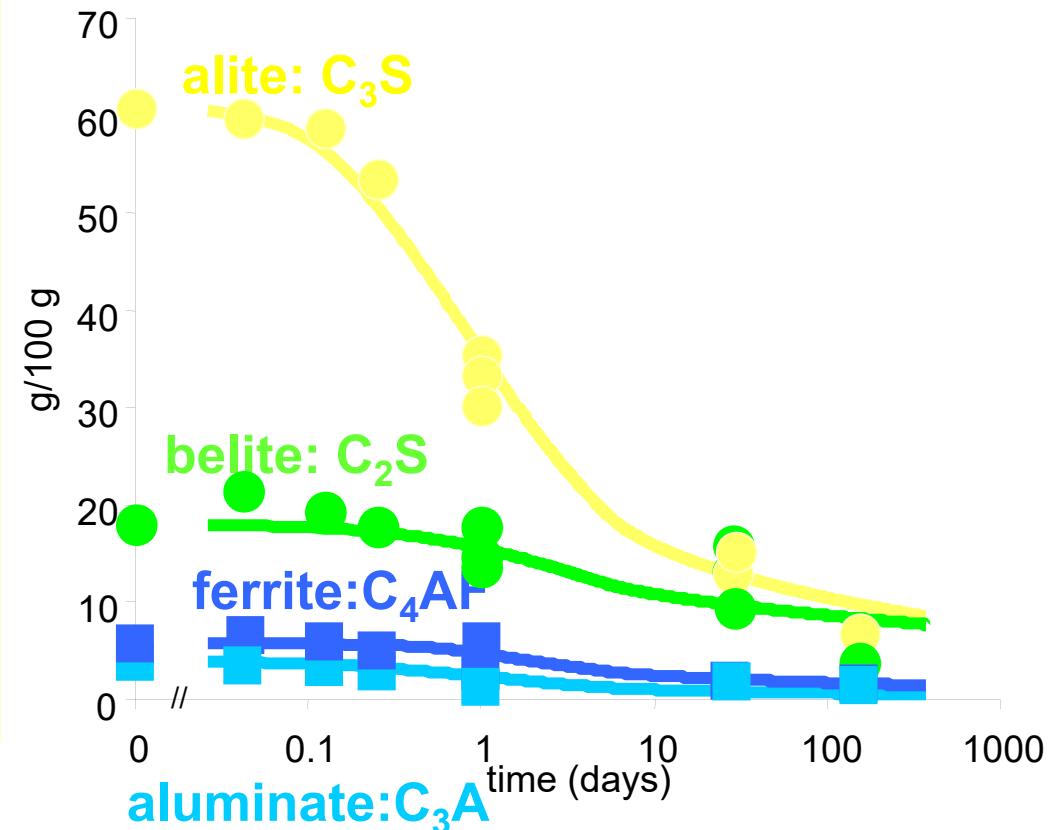
Empirical Approach: Parrot and Killoh (1984)

$$R_t = \frac{K_1}{N_1} (1 - \alpha_t) (-\ln(1 - \alpha_t))^{(1 - N_1)}$$

$$R_t = \frac{K_2 \times (1 - \alpha_t)^{2/3}}{1 - (1 - \alpha_t)^{1/3}}$$

$$R_t = K_3 \times (1 - \alpha_t)^{N_3}$$

All parameters (K_i, N_i) from
Parrot and Killoh (1984)



Cement specific input: surface area, w/c, composition

Modeling: Dissolution

Empirical Approach: Parrot and Killoh (1984)

nucleation

$$R_t = \frac{K_1}{N_1} (1 - \alpha_t) (-\ln(1 - \alpha_t))^{(1 - N_1)}$$

$$R_t = \frac{K_2 \times (1 - \alpha_t)^{2/3}}{1 - (1 - \alpha_t)^{1/3}} \quad \text{i} \text{diffusion}$$

$$R_t = K_3 \times (1 - \alpha_t)^{N_3} \quad \text{i shell}$$

degree of hydration

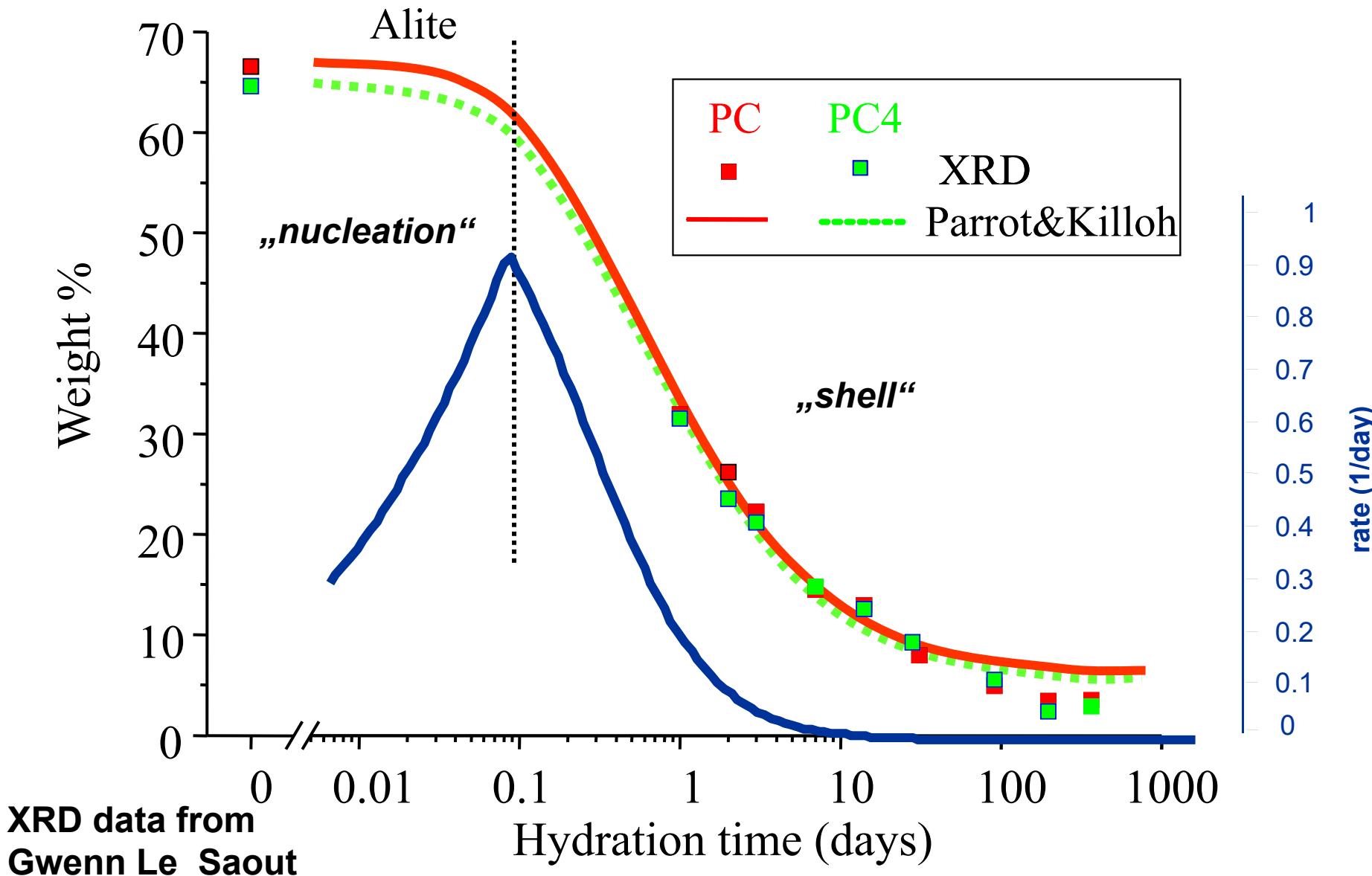
$$\alpha_t = \alpha_{t-1} + \Delta t \cdot R_{t-1} \cdot (1 + 3.333 \cdot (H \cdot w/c - \alpha_t))^4$$

for $\alpha_t > H \cdot w/c$.

	elite	belite	alum.	ferrite
K ₁	1.5	0.5	1.0	0.37
N ₁	0.7	1.0	0.85	0.7
K ₂	0.05	0.006	0.04	0.015
K ₃	1.1	0.2	1.0	0.4
N ₃	3.3	5.0	3.2	3.7
H	1.33	1.33	1.33	1.33

**Cement specific input:
surface area, w/c**

Modeling: Dissolution



Modeling: Dissolution

Empirical Approach: Parrot and Killoh adapted
Lothenbach et al. (2008) 38, 848-860

nucleation

$$R_t = \frac{K_1}{N_1} (1 - \alpha_t) (-\ln(1 - \alpha_t))^{(1 - N_1)}$$

$$R_t = \frac{K_2 \times (1 - \alpha_t)^{2/3}}{1 - (1 - \alpha_t)^{1/3}}$$

diffusion

$$R_t = K_3 \times (1 - \alpha_t)^{N_3}$$

shell

degree of hydration

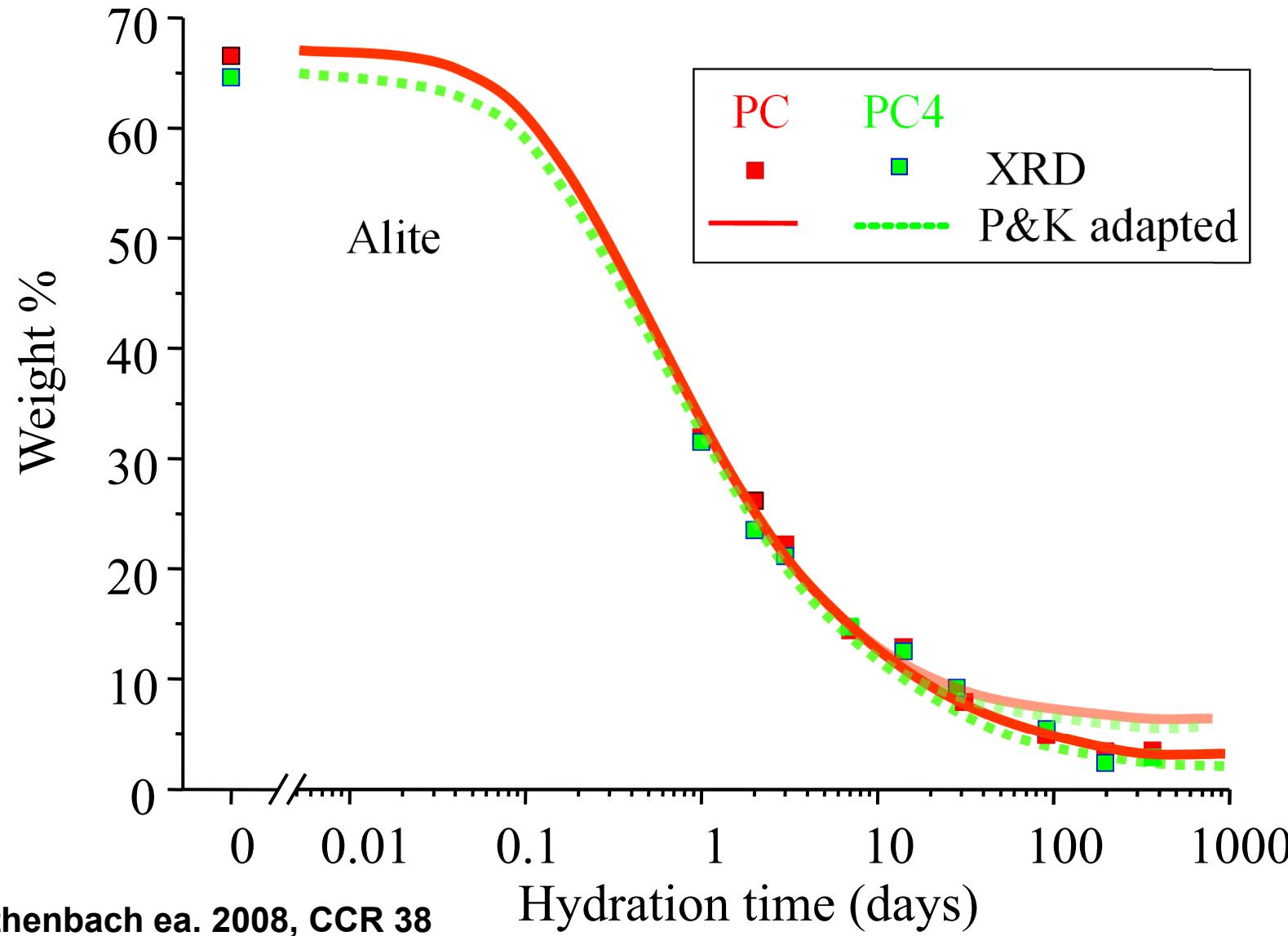
$$\alpha_t = \alpha_{t-1} + \Delta t \cdot R_{t-1} \cdot (1 + 3.333 \cdot (H \cdot w/c - \alpha_t))^4$$

for $\alpha_t > H \cdot w/c$.

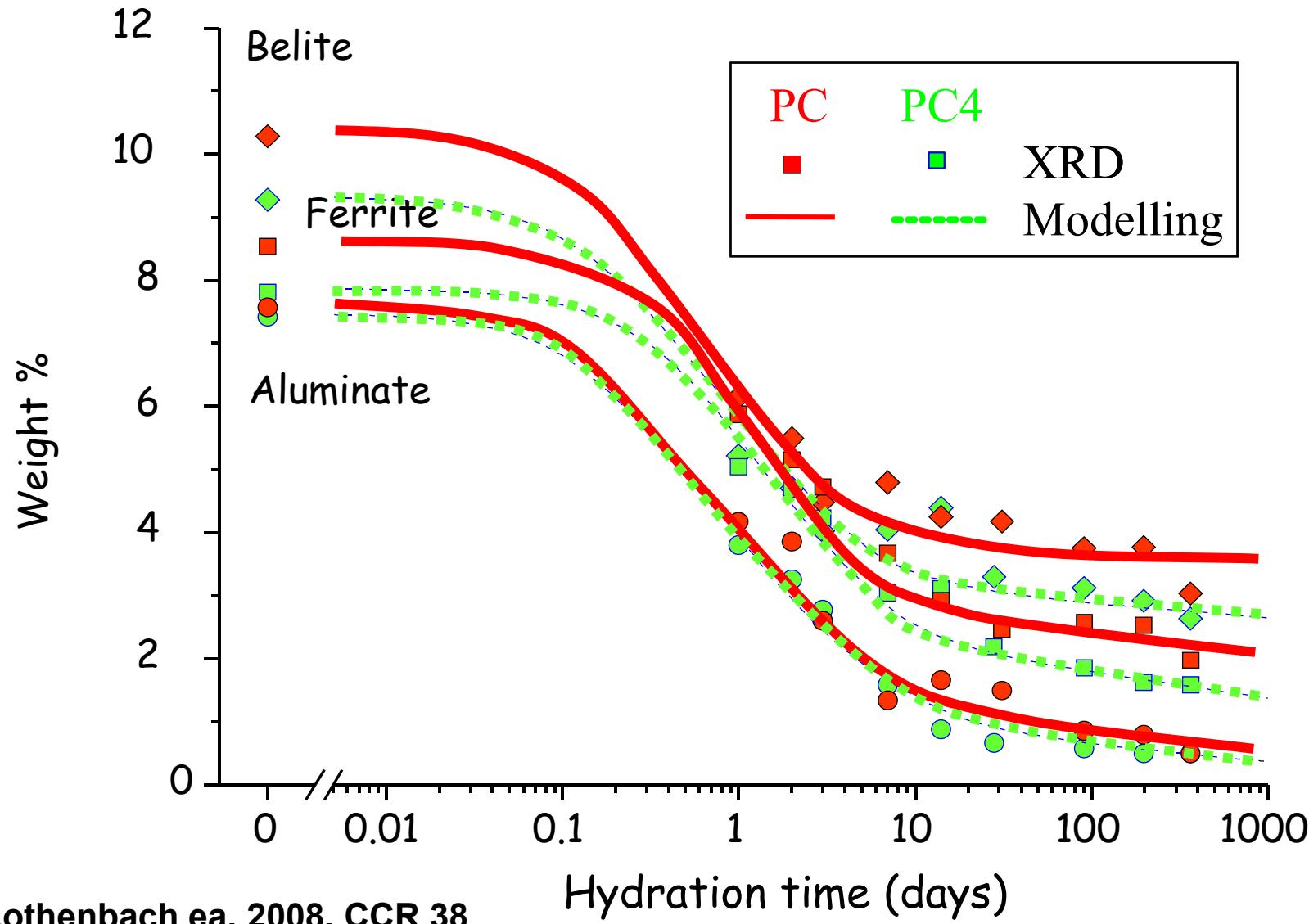
	alite	belite	alum.	ferrite
K ₁	1.5	0.5	1.0	0.37
N ₁	0.7	1.0	0.85	0.7
K ₂	0.05	0.02	0.04	0.015
K ₃	1.1	0.7	1.0	0.4
N ₃	3.3	5.0	3.2	3.7
H	2.0	1.55	1.8	1.65

**Cement specific input:
surface area, w/c**

Modeling: Dissolution



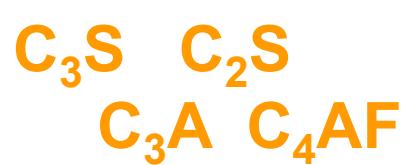
Modeling: Dissolution



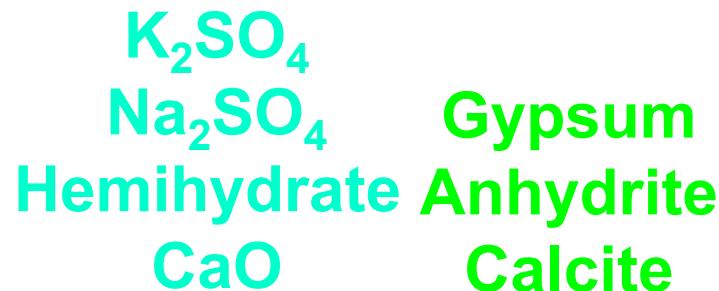
Thermodyn. calculations

Multi-component input

I Slowly soluble clinkers



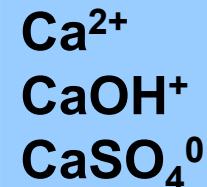
II Soluble solids



III Water



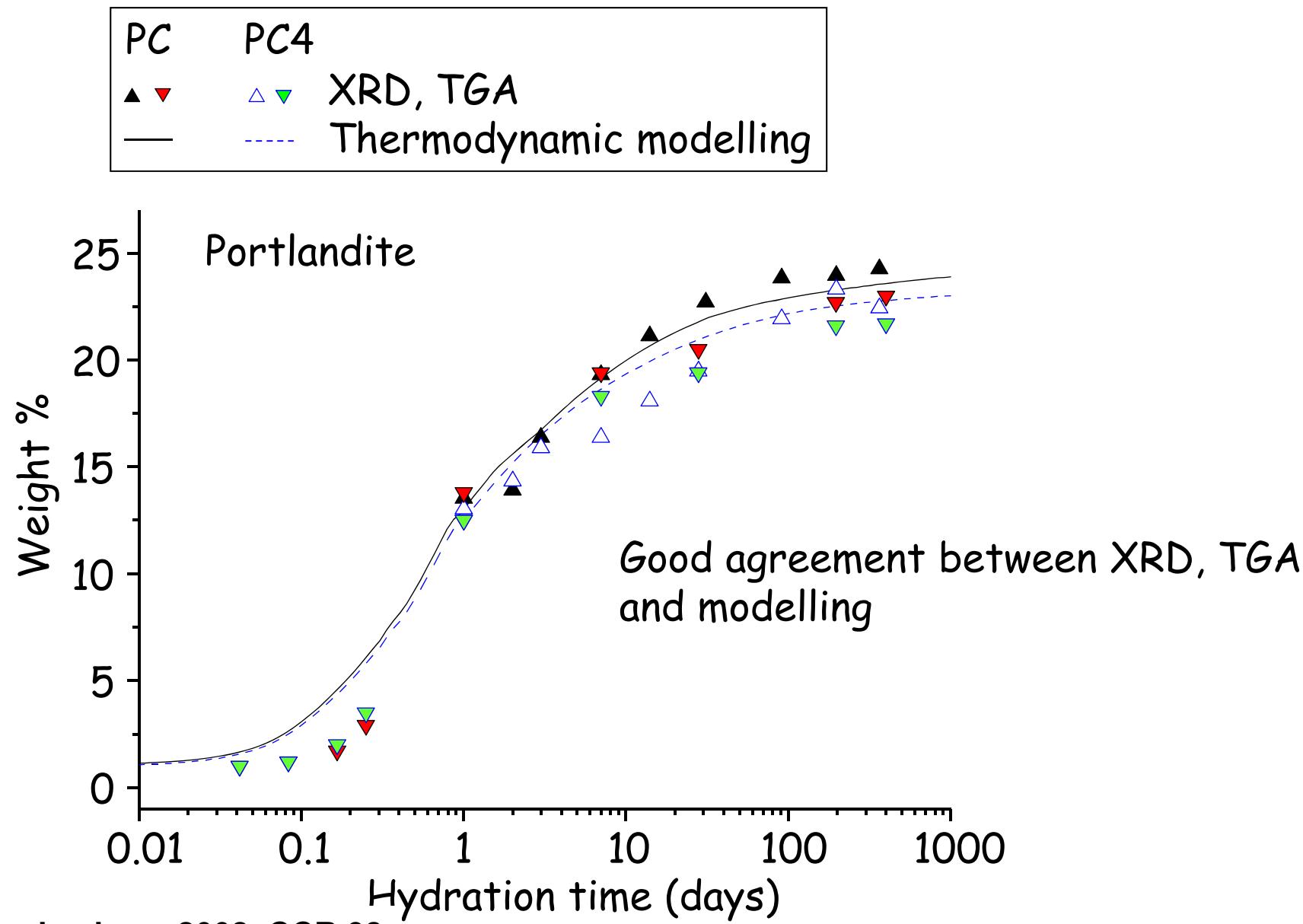
Thermodynamic modeling GEMS-PSI



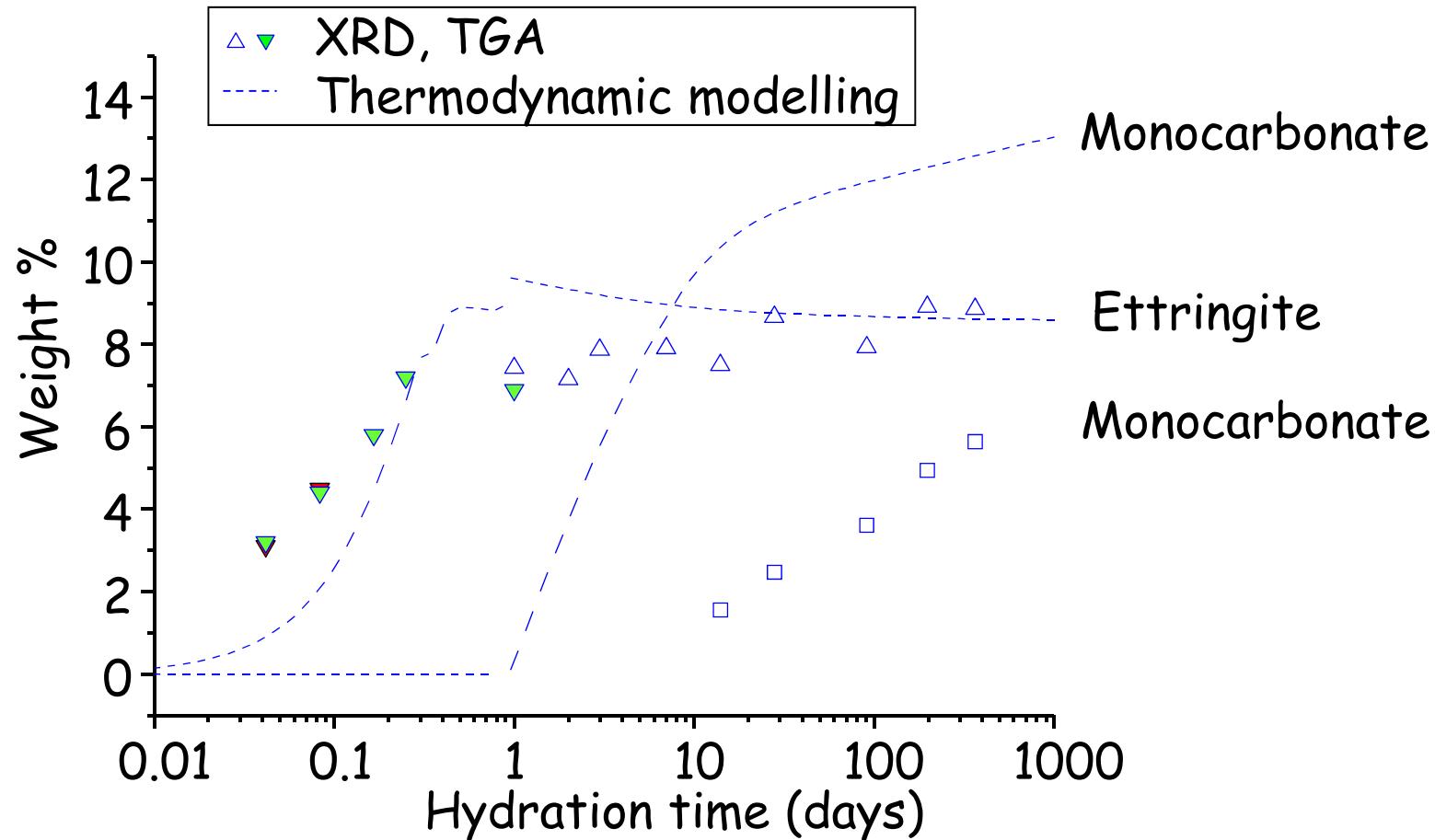
Speciation in solution



Output data, Portlandite



Output data, AFt, AFm phases



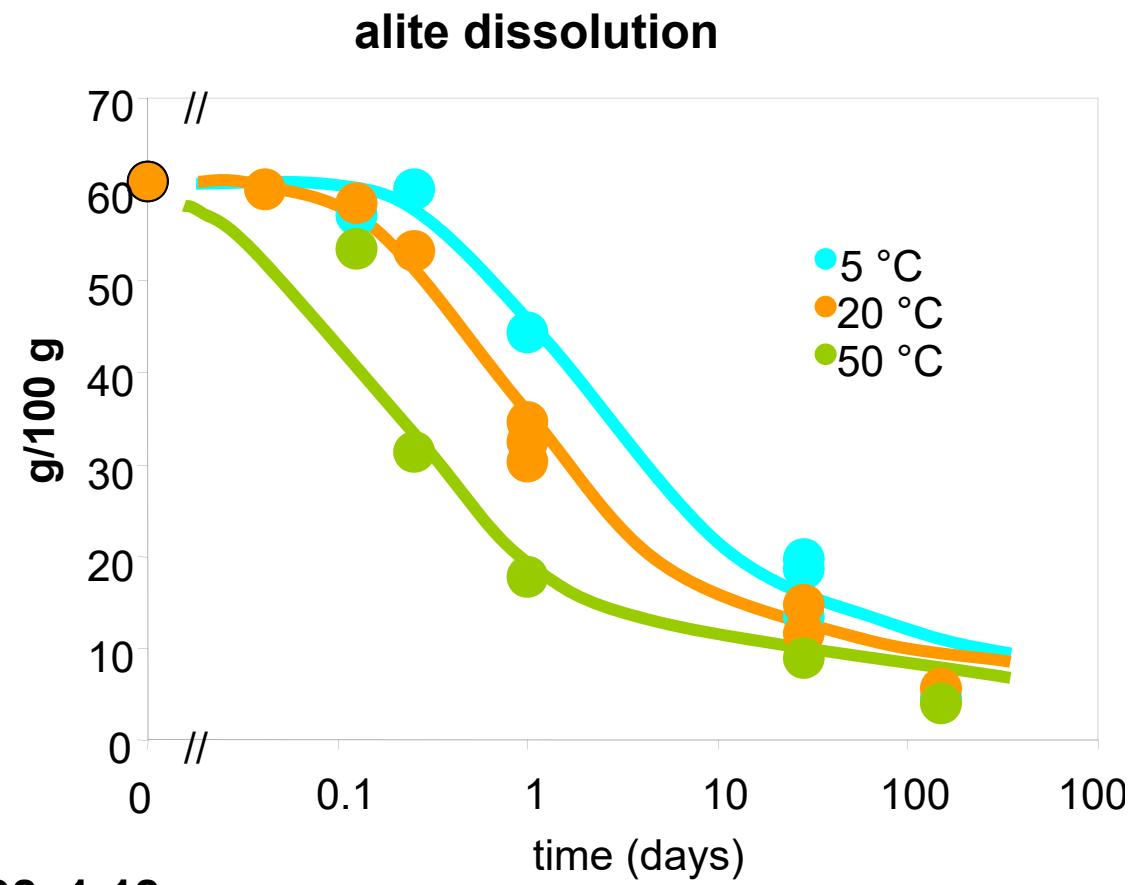
- Overestimation of monocarbonate (<= hemicarbonate, Al in C-S-H)
- Correct amount of ettringite in the PC sample

Modeling: Temperature

Arrhenius equation

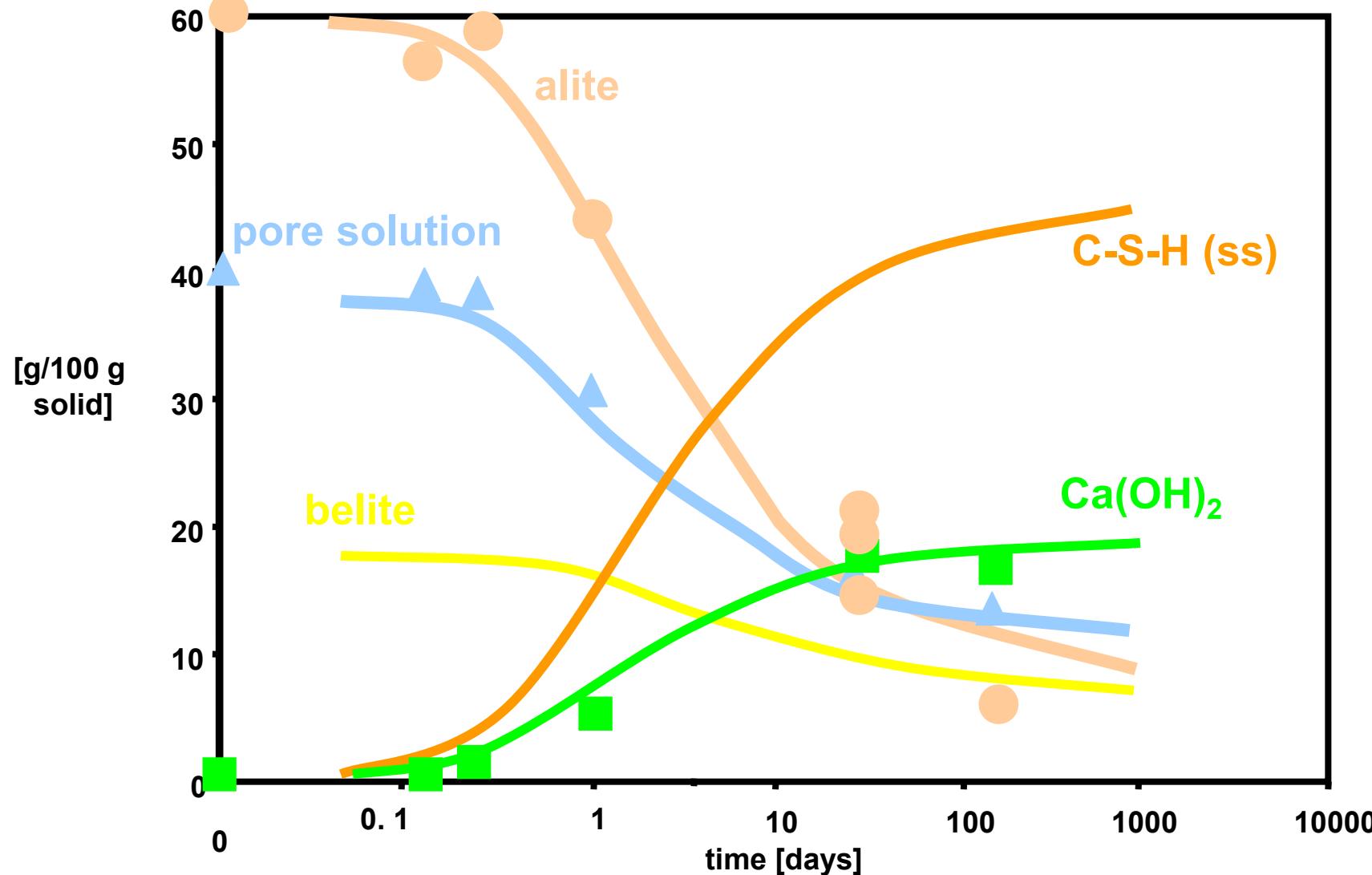
$$R_T = A e^{-\frac{E_a}{RT}}$$

E_a : literature

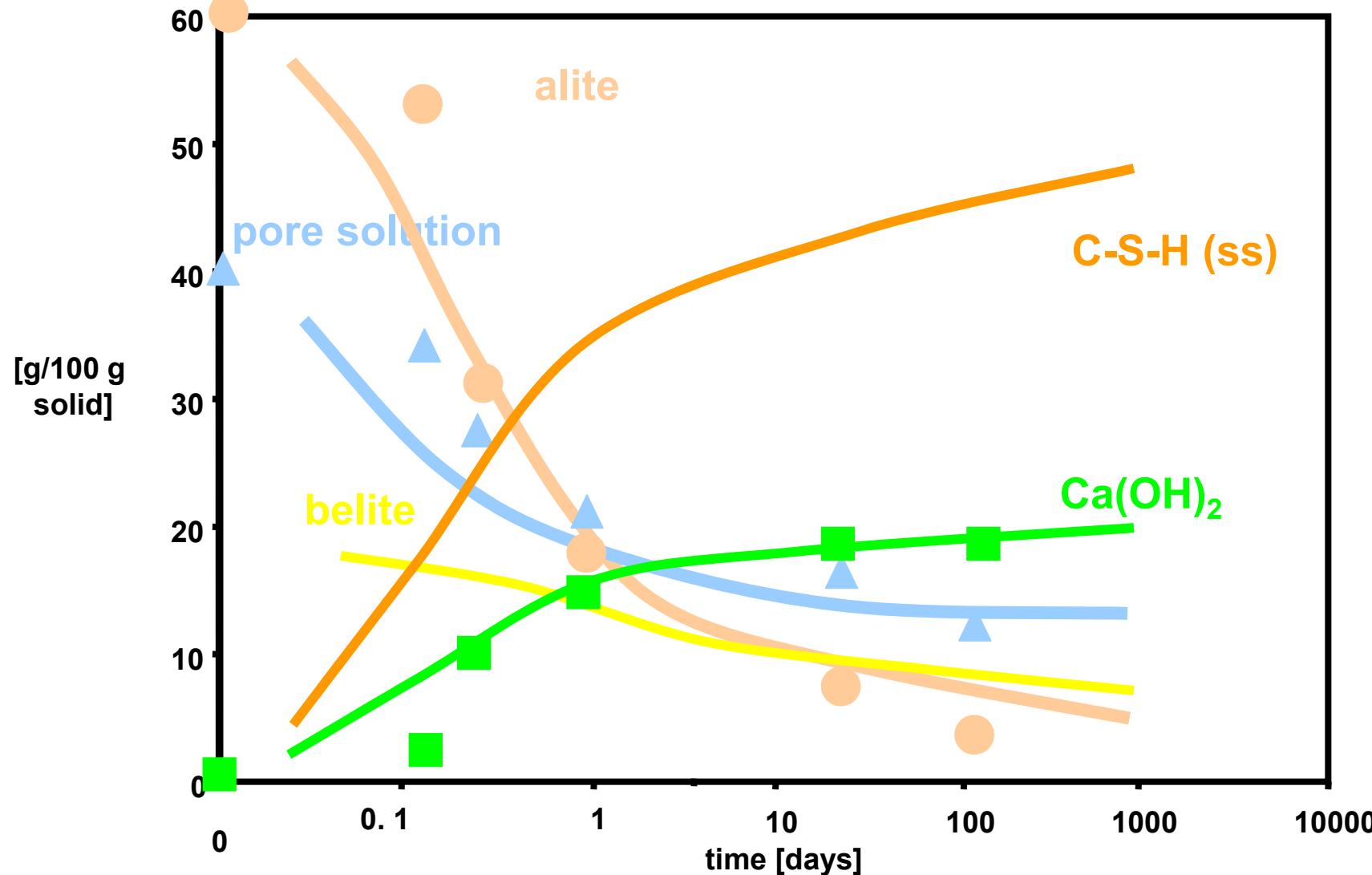


Lothenbach et al. (2008) CCR 38, 1-18

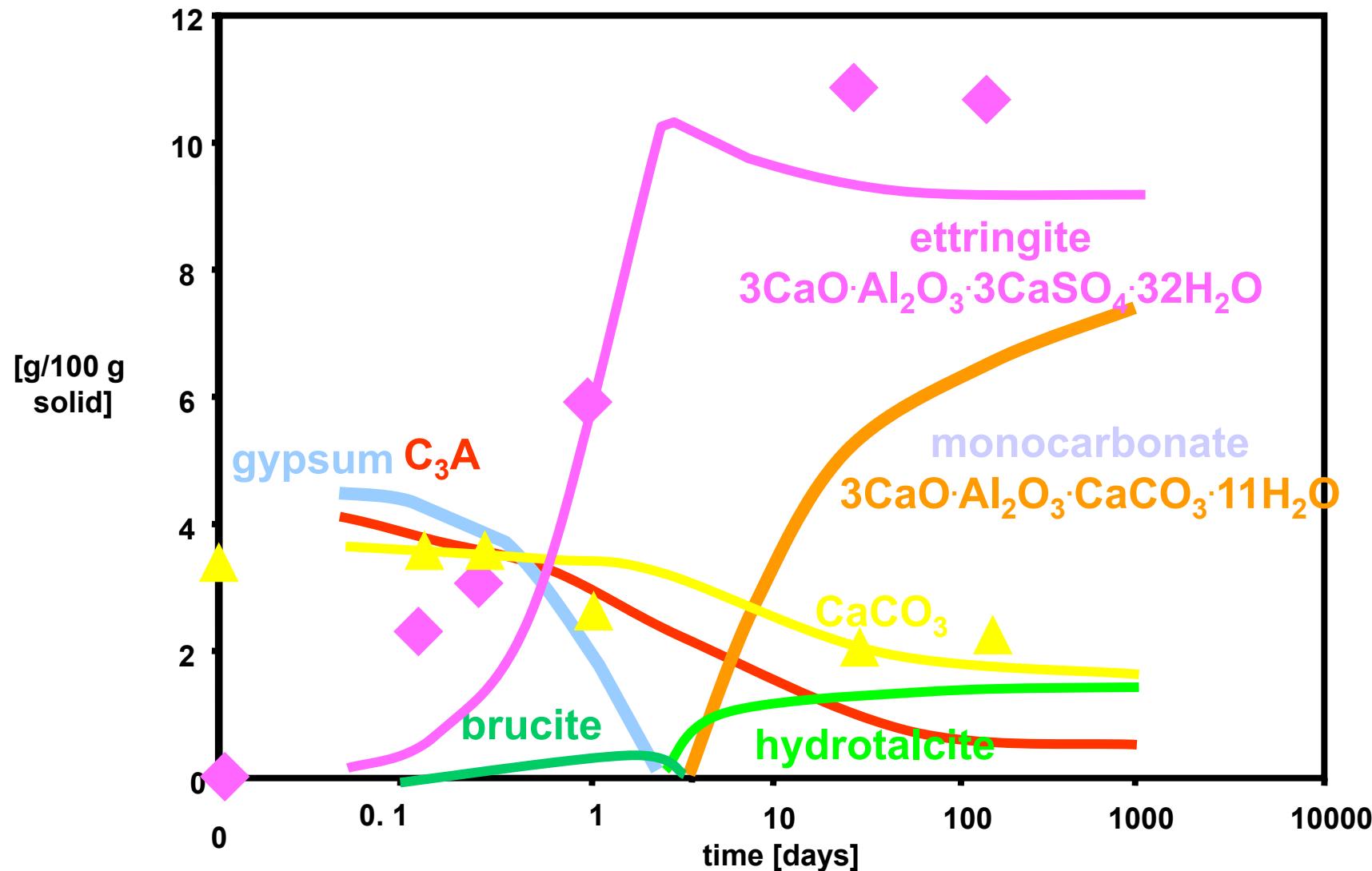
Ca- and Si-hydrates: 5 °C



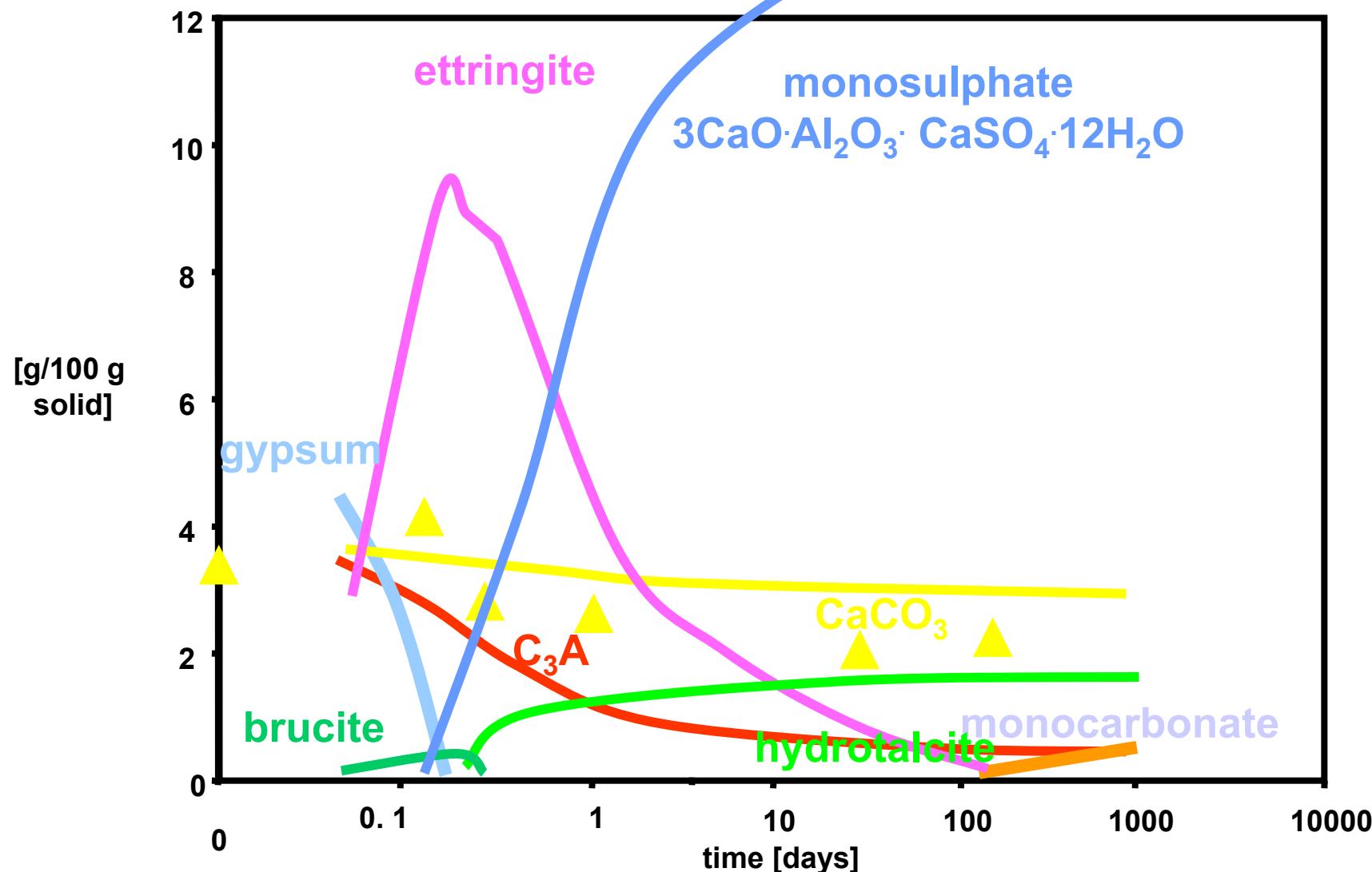
Ca- and Si-hydrates: 50 °C



Al-, SO₄-, CO₃: 5 °C



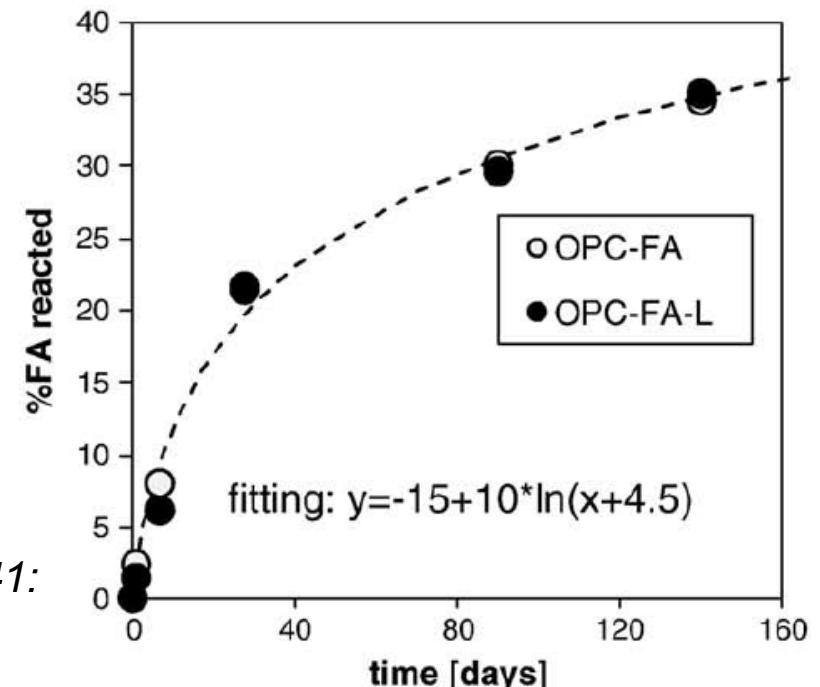
Al-, SO₄-, CO₃: 50 °C



Conclusion

- Empirical approach of P&K (adapted)
 - Describes observed dissolution (> 1 day) in OPC well
 - Simple to use
 - Influencing parameters: **surface area, w/c, temperature**
 - Purely empirical, other models can be used
 - Other influences: pH, composition of pore solution, ... not included

- Other models can be used
 - Any (empirical) equation which describes the reaction of solid as a function of time



De Weerdt ea (2011) CCR 41:
Reaction degree of fly ash

Modeling: Dissolution

$$R_{t,T} = \frac{K_1}{N_1} (1 - \alpha_t) (-\ln(1 - \alpha_t))^{(1-N_1)} \left(\frac{rh - 0.55}{0.45} \right)^4 e^{-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_0} \right)}$$

$$R_{t,T} = \frac{K_2 \times (1 - \alpha_t)^{2/3}}{1 - (1 - \alpha_t)^{1/3}} \left(\frac{rh - 0.55}{0.45} \right)^4 e^{-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_0} \right)}$$

$$R_{t,T} = K_3 \times (1 - \alpha_t)^{N_1} \left(\frac{rh - 0.55}{0.45} \right)^4 e^{-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_0} \right)}$$

Relative surface area factor
used for „nucleation and growth“ only
(relative to Dalziel & Gutteridge, 1986)

Influence of temperature
Arrhenius equation
Ea values: Lothenbach et al., 2008

Influence of the relative humidity
as proposed in Parrot and Killoh, 1984

Hydration in closed systems: rh = 1

Cement specific input: surface area [m²/kg], w/c, composition

Modeling: Dissolution

$$R_{t,T} = \frac{K_1}{N_1} (1 - \alpha_t) (-\ln(1 - \alpha_t))^{(1-N_1)} \left(\frac{rh - 0.55}{0.45} \right)^4 \frac{\text{surface area}}{385} e^{-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_0} \right)}$$

$$R_{t,T} = \frac{K_2 \times (1 - \alpha_t)^{2/3}}{1 - (1 - \alpha_t)^{1/3}} \left(\frac{rh - 0.55}{0.45} \right)^4 e^{-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_0} \right)}$$

$$R_{t,T} = K_3 \times (1 - \alpha_t)^{N_3} \left(\frac{rh - 0.55}{0.45} \right)^4 e^{-\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_0} \right)}$$

degree of hydration of each clinker phase

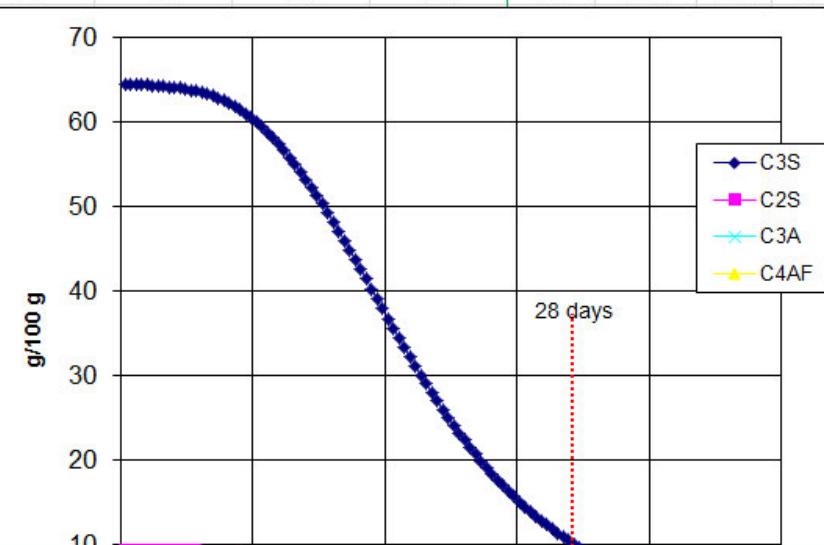
- *initial* $\alpha_t = \alpha_{t-1} + \Delta t \cdot R_{t-1}$
- *later, for $\alpha_{t-1}(\text{total}) > H \cdot w/c$;*
 $H \cdot w/c$ = critical degree of hydration

$$\alpha_t = \alpha_{t-1} + \Delta t \cdot R_{t-1} \cdot (1 + 3.333 \cdot (H \cdot w/c - \alpha_t))^4$$

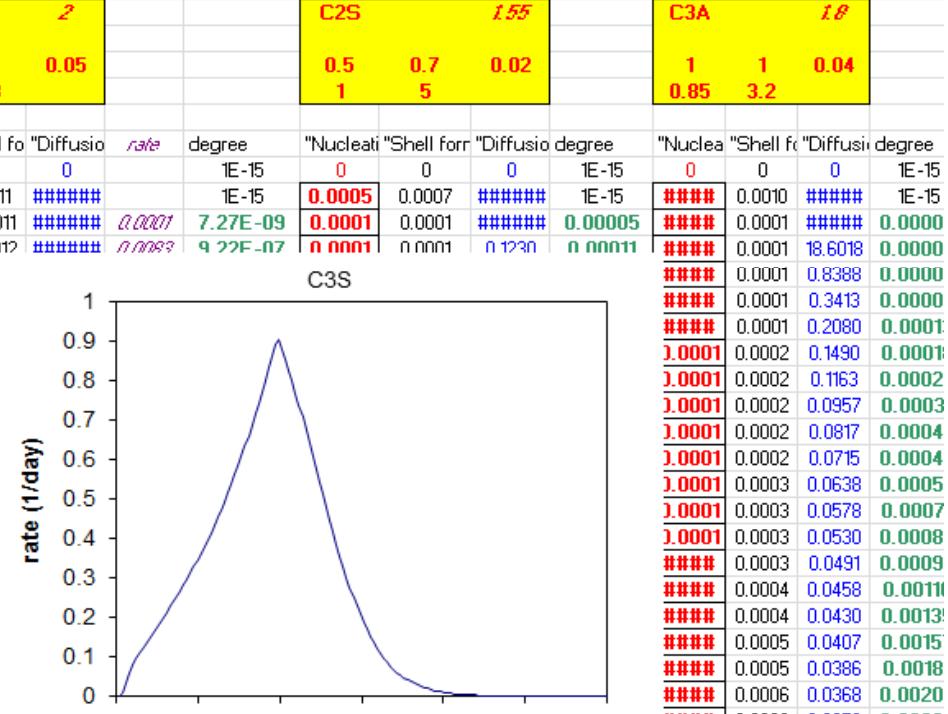
**Hydration is
reduced with time
at low w/c**

Cement specific input: surface area [m²/kg], w/c, composition

Parrot and Killoh model as Excel file



	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T
3	Reference area		385	C2S	9.3	20785														
4	wz		0.4	C3A	7.4	54040														
5	Temperature		20	C4AF	7.8	34087														
6			293.15																	
7	reference temp		293.15	r.h.	1.0	relative humidity (not tested for rh < 1)														
8	R		8.314																	
9	Notes																			
10	Enter your values in the "yellow" boxes; if necessary adapt K,N and H values (ungroup rows)																			
11	This calculation tool is not thoroughly tested. In case of errors please contact barbara.lothenbach@empa.ch																			
12	Original Model from Parrot and Killough (1984) Br Ceram Proc 35, 41-53																			
13	Ea and temperature dependence from Lothenbach et al (2008), Cem Concr Res 38, 1-18																			
14	Adapted K,N and H from Lothenbach et al. (2008) Cem Concr Res 38, 848-860																			
15	If you use this model cite the above publications																			
16																				
17																				
18																				
19																				
20	time (days)																			
21	0.00	4.16E-11	6.46E-14	9.28E-15	7.42E-15	7.81E-15														
22	0.02	0.0000	6.46E-14	9.28E-15	7.42E-15	7.81E-15														
23	0.03	0.0011	4.69E-07	0.00049775	5.2653E-06	1.4E-08														
24	0.03	0.0012	5.96E-05	0.00104524	0.00012844	1.1719E-06														
25	0.03	0.0013	0.000337	0.00164744	0.00034721	5.9793E-06														
26	0.04	0.0015	0.000852	0.00230982	0.00062657	1.4602E-05														
27	0.04	0.0016	0.001599	0.00303839	0.00096231	2.6999E-05														
28	0.04	0.0018	0.002591	0.00383975	0.00135615	4.3398E-05														
29	0.05	0.0019	0.003853	0.00472117	0.00181223	6.4197E-05														
30	0.05	0.0021	0.005417	0.00569064	0.00233619	8.9928E-05														
31	0.06	0.0024	0.007322	0.00675695	0.00293488	0.00012124														
32	0.06	0.0026	0.009616	0.00792975	0.00361632	0.00015892														
33	0.07	0.0029	0.012353	0.00921968	0.00438969	0.00020387														
34	0.08	0.0031	0.0156	0.01063839	0.0052654	0.00025715														
35	0.08	0.0035	0.01943	0.01219874	0.00625522	0.00031998														
36	0.09	0.0038	0.02393	0.01391483	0.00737238	0.00039379														
37	0.10	0.0042	0.029198	0.01580218	0.00863175	0.00048019														
38	0.11	0.0046	0.03535	0.01787785	0.01004999	0.00058105														
39	0.12	0.0051	0.042515	0.02016057	0.01164579	0.00069853														
40	0.13	0.0056	0.050845	0.02267095	0.01344004	0.0008351														
41	0.15	0.0061	0.060512	0.02543161	0.01545615	0.00099359														
42	0.16	0.0067	0.071715	0.02846743	0.01772028	0.00117725														
43	0.18	0.0074	0.08468	0.03180574	0.02026171	0.00138983														
44	0.20	0.0081	0.099667	0.03547656	0.02311314	0.00163559														
45	0.21	0.0090	0.116977	0.03951285	0.02631114	0.00191945														
46	0.24	0.0098	0.13695	0.04395084	0.02989656	0.00224705														
47	0.26	0.0108	0.159977	0.04883028	0.03391501	0.00262484														



Hydration modelling EXCEL + GEMS

1. Open project Parrot

Input Recipe of Single Thermodynamic System: Parrot:G:PC:0:0:1:20:0:

tname Hydration of PC

Property	Selection	Recipe Input
Compos (xa)		
DComp (xd)		
IComp (bi)		
Phase (xp)		
Kin.lower (d)		
Kin.upper (c)		
G0 shift (gE)		
Other Input		
C12A7		
C2S	M15SH C4AH13 C4ACIH10 Anh	1 xa_ MgO 0.87 g
C3A	AlOHam C4AH19 C4AsClH12 Gp	2 xa_ O2 1 g
C3S	AlOHmic CAH10 ettringite13 hemihydrate	3 xa_ SO3 0.0001 g
C4AF	Gbs monosulphate10.5 ettringite9 thaumasite	4 xd_ H2O@ 40 g
CA	Kln monosulphate12 Arg Fe	5 xd_ C2S 9.3 g
CA2	Gr monosulphate14 Cal FeCO3(pr)	6 xd_ C3A 7.4 g
C2AH7.5	C12A7 monosulphate16 C3FH6 Sd	7 xd_ C3S 64.5 g
C3AH6	C2S monosulphate9 C4FH13 Hem	8 xd_ C4AF 7.8 g
C4AH11	C3A chabazite C3FS0.84H4.32 Mag	9 xd_ Cal 4.57 g
	C3S zeoliteP_Ca C3FS1.34H3.32 Fe(OH)3(am)	10 xd_ Lim 0.89 g
	C4AF straetlingite5.5 Fe-hemicarbonate FeOOHmic	11 xd_ Anh 1e-09 g
	CA monocarbonate9 Femonocarbonate Gt	12 xd_ Gp 3 g
	CA2 hemicarbonat10.5 Dis-Dol Py	13 xd_ hemihyd... 1e-09 g
	C2AH7.5 hemicarbonate Ord-Dol Tro	14 xd_ K2SO4 1.28 g
	C3AH6 hemicarbonate9 Lim Melanterite	
	C4AH11 monocarbonate Portlandite K2SO4	

Input quantities of Dependent Components stoichiometries contributing to B_{vector}

Learn more Print OK Cancel

All input in g
(100 g cement)

hydratio:G:PC:0:0:1:20:0:aqueous:S:

Controls Sampling Results Config 11/05/2017, 12:57

OPC with limestone

Parrot and Killoh adapted according Lothenbach et al. 2008

	iTm	iV	iP	iTC	iNv	iTau	ipXi	iNu	i
0	1000	0	1	20	0	0	0	0	0
1	1501	0	1	20	0	0	0	500	0
2	1	0	0	0	0	0	0	1	0
cTm	1128	0	1	20	0	0	0	0	128

Reaction from Excel

	Time (days)	Reacted C3S
0	0	0
1	0	0
2	0	0
3	0	0
4	0	0
5	0	0
6	0	0
7	0	0
8	0	0
9	0	0
10	0	0
11	0	0
12	0	0
...

; Parrot and Killoh adapted (H set to 2, 1.55, 1.8 and 1.65), influence ...
 ; Clinker phases from Bogue calculations (in case of Rietveld data correc...
 ; cement specific input; enter data as [g/100g]
 ;surface area (m²/kg)
 nodC[0][5] =: 413;
 ;w/z
 nodC[1][5] =: 0.40;
 ;C3S (in g/100g)
 nodC[2][5] =: 64.64;
 ;C2S (in g/100g)
 nodC[3][5] =: 9.28;
 ;C3A (in g/100g)
 nodC[4][5] =: 7.42;
 ;C4AF (in g/100g)
 nodC[5][5] =: 7.81;
 ; calcite
 zd_{Cal} =: 4.57;
 ; free lime
 zd_{Lim} =: 0.89;
 ; gypsum
 zd_{Gn} =: 3;

Cement specific input

	modC[0]	modC[1]	modC[2]
0	4.16667e-011	6.46e-014	9.2
1	0.001	6.46e-014	9.2
2	0.0011	4.69473e-007	0.000
3	0.0012	5.95605e-005	0.001
4	0.0013	0.000337479	0.00
5	0.0015	0.000851873	0.002
6	0.0016	0.001598878	0.00
7	0.0018	0.002591409	0.003
8	0.0019	0.003853374	0.004
9	0.0021	0.00541697	0.005
10	0.0024	0.007321916	0.006
11	0.0026	0.009615555	0.007
12	0.0029	0.012353404	0.009
...

Architecture of GEMS file

- Input always in g/100g
- The amount of clinker reacted copied from EXCEL file
- Inputs needed in GEMS:
 - surface area [m²/kg]
 - w/c
 - C₃S, C₂S, C₃A, C₄AF (pure phases)
 - Calcite, free lime, gypsum, anhydrite, hemihydrate, periclase, Na₂SO₄ and K₂SO₄ (-> soluble alkalis)
 - Na₂O, K₂O, MgO and SO₃ in clinker (as g/g clinker)
optional

Architecture of GEMS file

- Process: controls below input
 - Ea (activation energy)
 - Conversion of different input parameter
 - Correction factors for minor elements in clinker
 - Amount of input water
 - Calculations of the dissolution of minor elements

Do not change!

Architecture of GEMS file

- Process: sampling: definition of output
 - X-axis: log (time)
 - Mass in g/100 g of hydrated cement
 - All data corrected from g/100 g unhydrated cement to g/100 g hydrated cement (corresponds to conditions of XRD, TGA measurements); can easily be changed, but you will have to convert XRD/TGA data
 - Amount of clinkers (with impurities)
 - Amount of hydrates (! Check single system file for the presence of additional solids and include them in the list)
 - Amount of pore solution (including dissolved species)

Check single system file for additional solids

Parrot:G:PC:0:0:1:20:0:mass:S:

Controls	Sampling	Results	Config	29/04/2019, 12:37		
cTau	0	cpXi	0	cXi	1	cNu
cpH	0	cpe	0	cEh	0	cT

```

$ Abscissa: log(time in days)
xp[J] := lg(modC[J][0]);
$ Ordinates (in g/100 g unhydrated cement)
$ clinker unreacted; include also minor elements
yp[J][0] := phM[{Alite}]/modC[24][5];
yp[J][1] := phM[{Belite}]/modC[25][5];
yp[J][2] := phM[{Aluminate}]/modC[26][5];
yp[J][3] := phM[{Ferrite}]/modC[27][5];
yp[J][4] := phM[{CSHQ}];
yp[J][5] := phM[{Portlandite}]; = C3S not reacted at time t
yp[J][6] := phM[{Gypsum}];
yp[J][7] := phM[{syngenite}];
yp[J][8] := phM[{Calcite}];
yp[J][9] := (phM[{ettringite}]+phM[{SO4_CO3_AFt}]+phM[{CO3_SO4_AFt}])+phM...
yp[J][10] := (phM[{C4AsH16}]+phM[{C4AsH14}]+phM[{SO4_OH_AFm}]+phM[{OH_SO...
yp[J][11] := phM[{C4AcH11}];
yp[J][12] := phM[{C4Ac0.5H12}];
yp[J][13] := phM[{straetlingite}];
yp[J][14] := phM[{C3AH6}];
yp[J][15] := phM[{OH-hydrotalcite}]+phM[{hydrotalc-pyro}];
yp[J][16] := phM[{C3(AF)S0.84H}]+phM[{C3FS0.84H4.32}]+phM[{C3FS1.34H3.32...];
yp[J][17] := phM[{Brucite}];
yp[J][18] := phM[{Ferrihydrite-mc}];
yp[J][19] := phM[{aq_gen}];

$correction to hydrated cement possible
$ / (1+modC[1][5]-phM[{aq_gen}]/100) = 1+0.4-mass H2O unreacted/100
$ = mass hydrated cement (after removal of pore water)

```

= C3S not reacted at time t
 $\text{modC}[24][5]$ correction for presence of
 minor elements in clinker; = 0.99 here

phM[{Portlandite}] -> mass of portlandite
 in g per 100 g unhydrated cement
 ! Spelling has to correspond exactly to
 single component!

$(1+\text{modC}[1][5]-\text{phM}[\{\text{aq_gen}\}]/100)$
 $= 1+0.4-\text{mass H}_2\text{O unreacted}/100$
 = mass hydrated cement
 (after removal of pore water)

For comparison with XRD/TGA

Controls Sampling Results Config 29/04/2019, 12:51

hydration of PC

Unit of x-axis

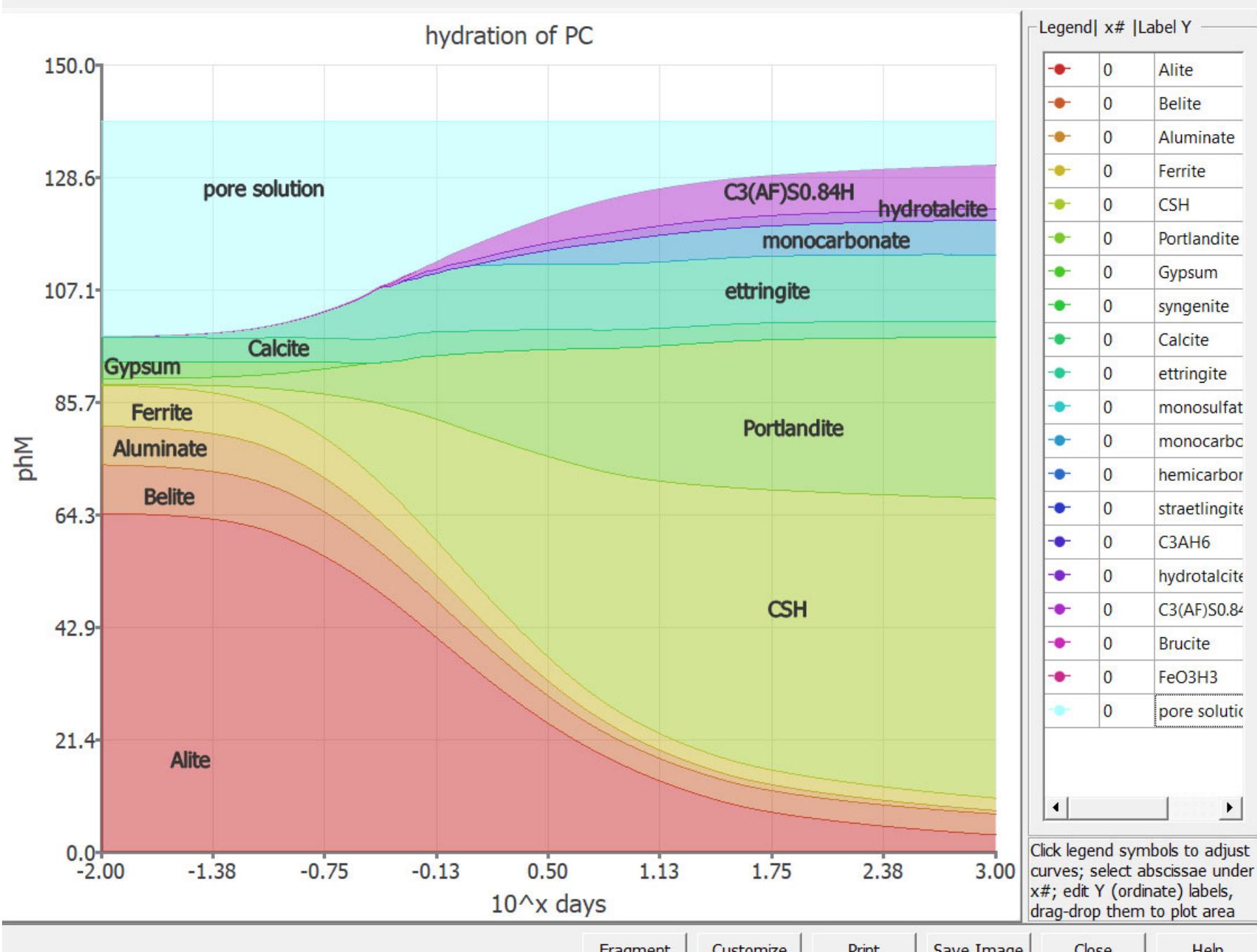
pX_Nam	10^x days	Alite	Belite	Aluminate	Ferrite	pY_Nam	phM
0	-10.380211	64.64	9.28	7.42	7.81		
1	-2.9586073	64.64	9.2795023	7.4199947	7.81		
2	-2.9208187	64.63994	9.2789548	7.4198716	7.8099988		
3	-2.8860566	64.639663	9.2783526	7.4196528	7.809994		
4	-2.8239087	64.639148	9.2776902	7.4193734	7.8099854		
5	-2.79588	64.638401	9.2769616	7.4190377	7.809973		
6	-2.7447275	64.637409	9.2761602	7.4186438	7.8099566		
7	-2.7212464	64.636147	9.2752788	7.4181878	7.8099358		
8	-2.6777807	64.634583	9.2743094	7.4176638	7.8099101		
9	-2.6197888	64.632678	9.273243	7.4170651	7.8098788		
10	-2.5850266	64.630384	9.2720702	7.4163837	7.8098411		
11	-2.537602	64.627647	9.2707803	7.4156103	7.8097961		
12	-2.5086383	64.6244	9.2693616	7.4147346	7.8097429		
13	-2.455932	64.62057	9.2678013	7.4137448	7.80968		
14	-2.4202161	64.61607	9.2660852	7.4126976	7.8096062		
15	-2.3854081	64.611607	9.2650252	7.4116976	7.80956062		

y-axis labels

**X-axis
Time
(10^x days)**

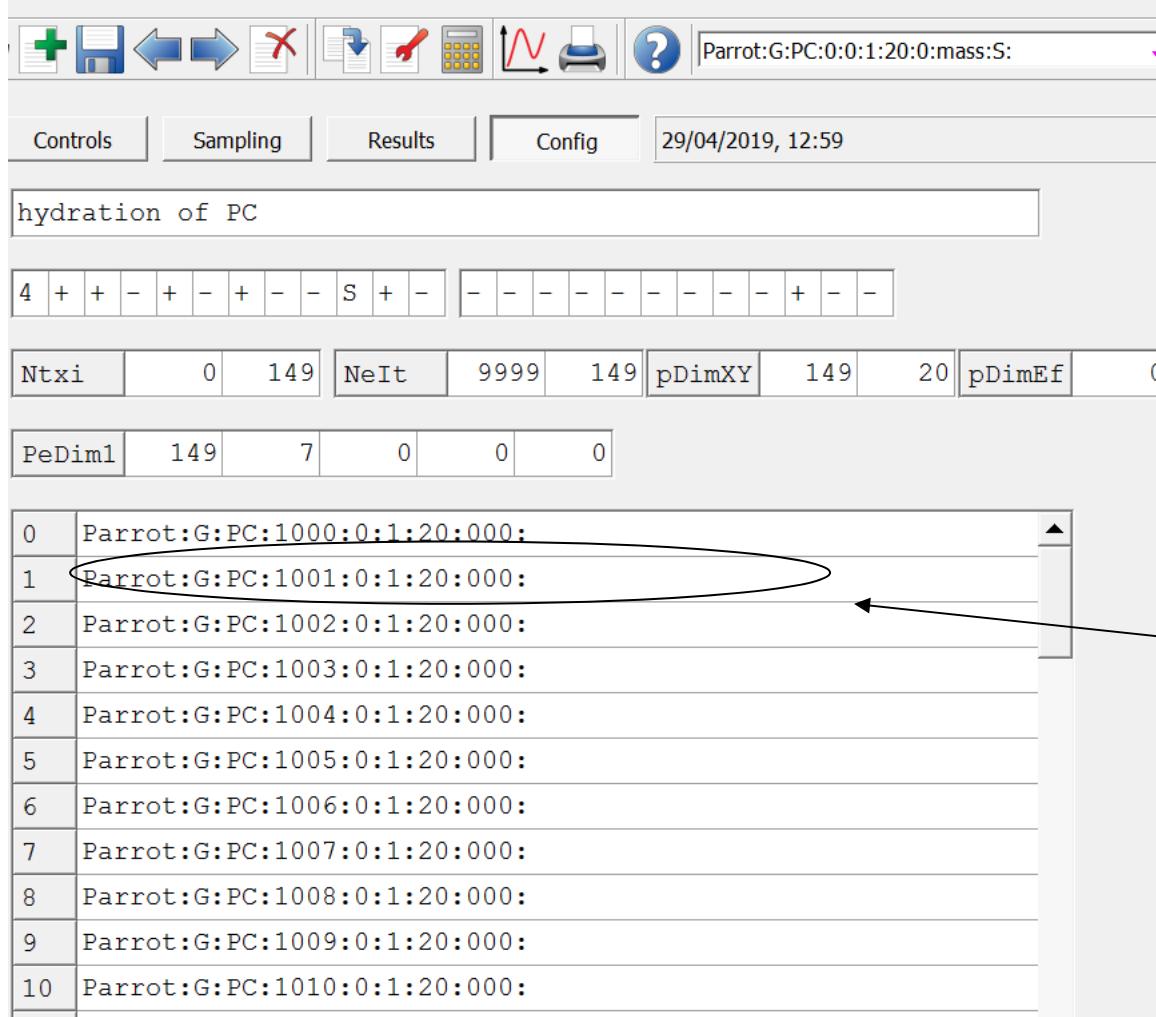
**y-axis
e.g. unreacted
clinker**

**(in g/100 g of
unhydrated
cement
as defined in
page sampling)**



Architecture of GEMS file

■ Process: Config: single system files



The screenshot shows the GEMS software interface in the 'Config' tab. The top bar displays various icons and the path 'Parrot:G:PC:0:0:1:20:0:mass:S:'. Below the toolbar, there are tabs for 'Controls', 'Sampling', 'Results', and 'Config', with 'Config' being the active tab. The date and time '29/04/2019, 12:59' are also shown. The main area contains several input fields and lists:

- A text input field containing 'hydration of PC'.
- An array input field with values: 4, +, +, -, +, -, S, +, -, -, -, -, -, -, -, +, -, -.
- Input fields for Ntxi (0), NeIt (149), pDimXY (9999), pDimXY (149), pDimEf (20), and pDimEf (0).
- An input field for PeDim1 (149, 7, 0, 0, 0).
- A list of generated files from index 0 to 10, all labeled 'Parrot:G:PC:1000:0:1:20:000:' followed by a unique identifier (e.g., 1, 2, 3, ...). The entry at index 1 is circled in black.

Name of the „parent file“
in „Single-System Equilibria“

Names of the „kid files“
produced:
The results of each calculation
can be checked

Architecture of GEMS file

- Process: Results: output
- X-axis: log (time)
 - Y-axis Mass in g/100 g of hydrated cement
- Experimental data, same format as calculated data
 - Number of data points can be adapted by „Record:Remake“
- Data used to prepare graph, can be exported to Excel or other softwares by copy/paste

Comparison with experimental data

Remake

Number of experimental points

Number of data categories

Selektor 3 (GEMS3) - Geochemical Equilibrium Model

File Record Window Help

Process

Parrot: *::*: *::*: *::*: *::*: *::*

	3	4	5	6	7	8	9
1	PC	0	0	1	20	0	Mass_corr
2	PC	0	0	1	20	0	mass

GEM-Selektor Process Setup: hydratio:G:PC:0:0:1:20:0:mass2:S:

Step 4 - Important data object dimensions

Spin boxes below define the dynamic memory configuration of the process.

Dimensions of sampled and experimental data

149	nPS - Number of steps (1 to 9999) to be performed in this simulation.
7	Number of 'modC' array columns (1 to 40, 0 - not used) to store nPS.
18	Number of columns in the 'yp' table (0 to 200) to keep the simulation results. The number of rows will be nPS.
1	Number of columns in the 'xp' table (0 to 4) to keep the simulation results. The number of rows will be nPS.
24	Number of rows in the xEp, yEp arrays for experimental data.
9	Number of columns in the xEp, yEp arrays for experimental data.

Optional data vectors (of length nPS) can be used for accumulating current values. They can be allocated using checkboxes below. The assignment operator (=) automatically copied into data vector from the respective process iteration.

Allocation of optional data vectors

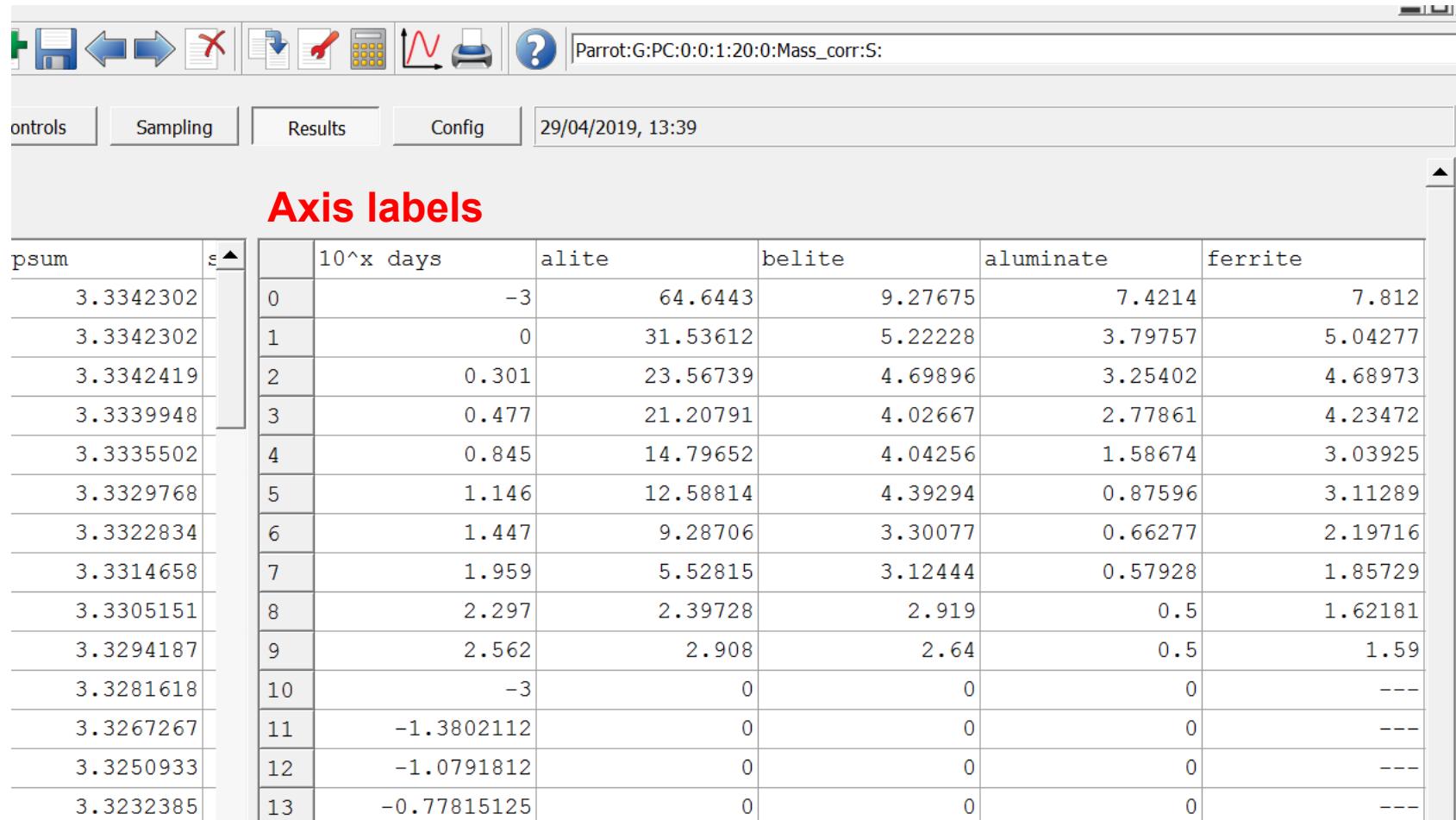
<input type="checkbox"/> CSD variant # ('vTm')	<input type="checkbox"/> Volume V, l ('vV')
<input type="checkbox"/> Temperature T ('vT')	<input type="checkbox"/> Constraints # ('vNV')
<input type="checkbox"/> Process extent pXi ('vpXi')	<input type="checkbox"/> Kinetic parameters ('vKin')

[Learn more](#)

Possibility to plot experimental data

See process Mass_corr

Experimental y-axis
(in g/100 g of unhydrated cement)

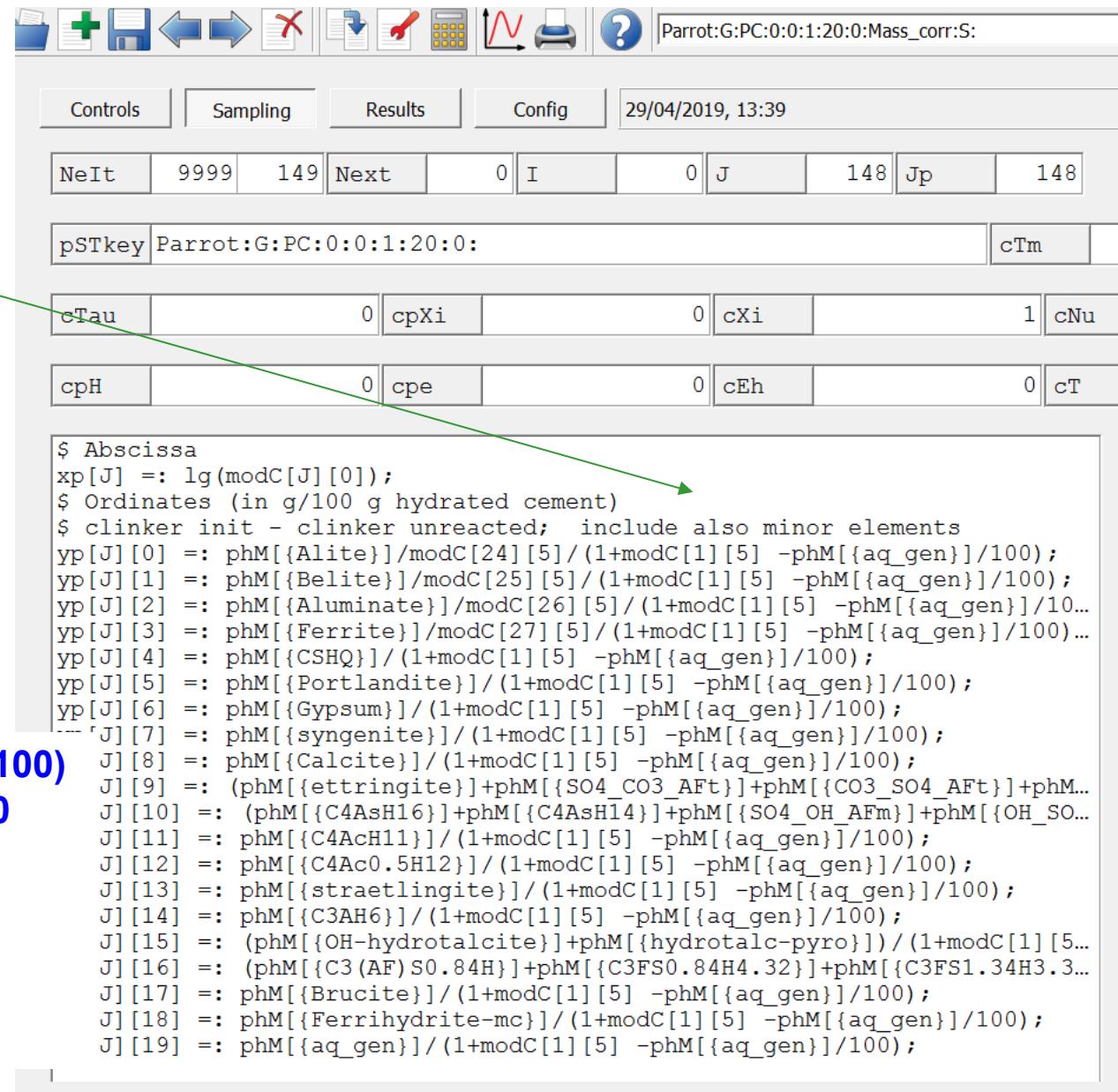


The screenshot shows a software interface with a toolbar at the top containing icons for file operations, sampling, results, and configuration. Below the toolbar, a header bar displays the path "Parrot:G:PC:0:0:1:20:0:Mass_corr:S:" and the date and time "29/04/2019, 13:39". The main area contains a table with the following data:

psum	10^x days	alite	belite	aluminate	ferrite
3.3342302	-3	64.6443	9.27675	7.4214	7.812
3.3342302	0	31.53612	5.22228	3.79757	5.04277
3.3342419	0.301	23.56739	4.69896	3.25402	4.68973
3.3339948	0.477	21.20791	4.02667	2.77861	4.23472
3.3335502	0.845	14.79652	4.04256	1.58674	3.03925
3.3329768	1.146	12.58814	4.39294	0.87596	3.11289
3.3322834	1.447	9.28706	3.30077	0.66277	2.19716
3.3314658	1.959	5.52815	3.12444	0.57928	1.85729
3.3305151	2.297	2.39728	2.919	0.5	1.62181
3.3294187	2.562	2.908	2.64	0.5	1.59
3.3281618	-3	0	0	0	---
3.3267267	-1.3802112	0	0	0	---
3.3250933	-1.0791812	0	0	0	---
3.3232385	-0.77815125	0	0	0	---

Experimental X-axis
Time (in log)

Comparison with experimental data



```
$ Abscissa
xp[J] := lg(modc[J][0]);
$ Ordinates (in g/100 g hydrated cement)
$ clinker init - clinker unreacted; include also minor elements
yp[J][0] := phM[{Alite}]/modC[24][5]/(1+modC[1][5]-phM[{aq_gen}]/100);
yp[J][1] := phM[{Belite}]/modC[25][5]/(1+modC[1][5]-phM[{aq_gen}]/100);
yp[J][2] := phM[{Aluminate}]/modC[26][5]/(1+modC[1][5]-phM[{aq_gen}]/100);
yp[J][3] := phM[{Ferrite}]/modC[27][5]/(1+modC[1][5]-phM[{aq_gen}]/100);
yp[J][4] := phM[{CSHQ}]/(1+modC[1][5]-phM[{aq_gen}]/100);
yp[J][5] := phM[{Portlandite}]/(1+modC[1][5]-phM[{aq_gen}]/100);
yp[J][6] := phM[{Gypsum}]/(1+modC[1][5]-phM[{aq_gen}]/100);
---'J][7] := phM[{syngenite}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][8] := phM[{Calcite}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][9] := (phM[{ettringite}]+phM[{SO4_CO3_AFt}])+phM[{CO3_SO4_AFt}]+phM...
J][10] := (phM[{C4AsH16}]+phM[{C4AsH14}])+phM[{SO4_OH_AFm}]+phM[{OH_SO...
J][11] := phM[{C4ACh11}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][12] := phM[{C4Ac0.5H12}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][13] := phM[{straetlingite}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][14] := phM[{C3AH6}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][15] := (phM[{OH-hydrotalcite}]+phM[{hydrotalc-c-pyro}])/(1+modC[1][5]...
J][16] := (phM[{C3(AF)S0.84H}]+phM[{C3FS0.84H4.32}])+phM[{C3FS1.34H3.3...
J][17] := phM[{Brucite}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][18] := phM[{Ferrihydrite-mc}]/(1+modC[1][5]-phM[{aq_gen}]/100);
J][19] := phM[{aq_gen}]/(1+modC[1][5]-phM[{aq_gen}]/100);
```

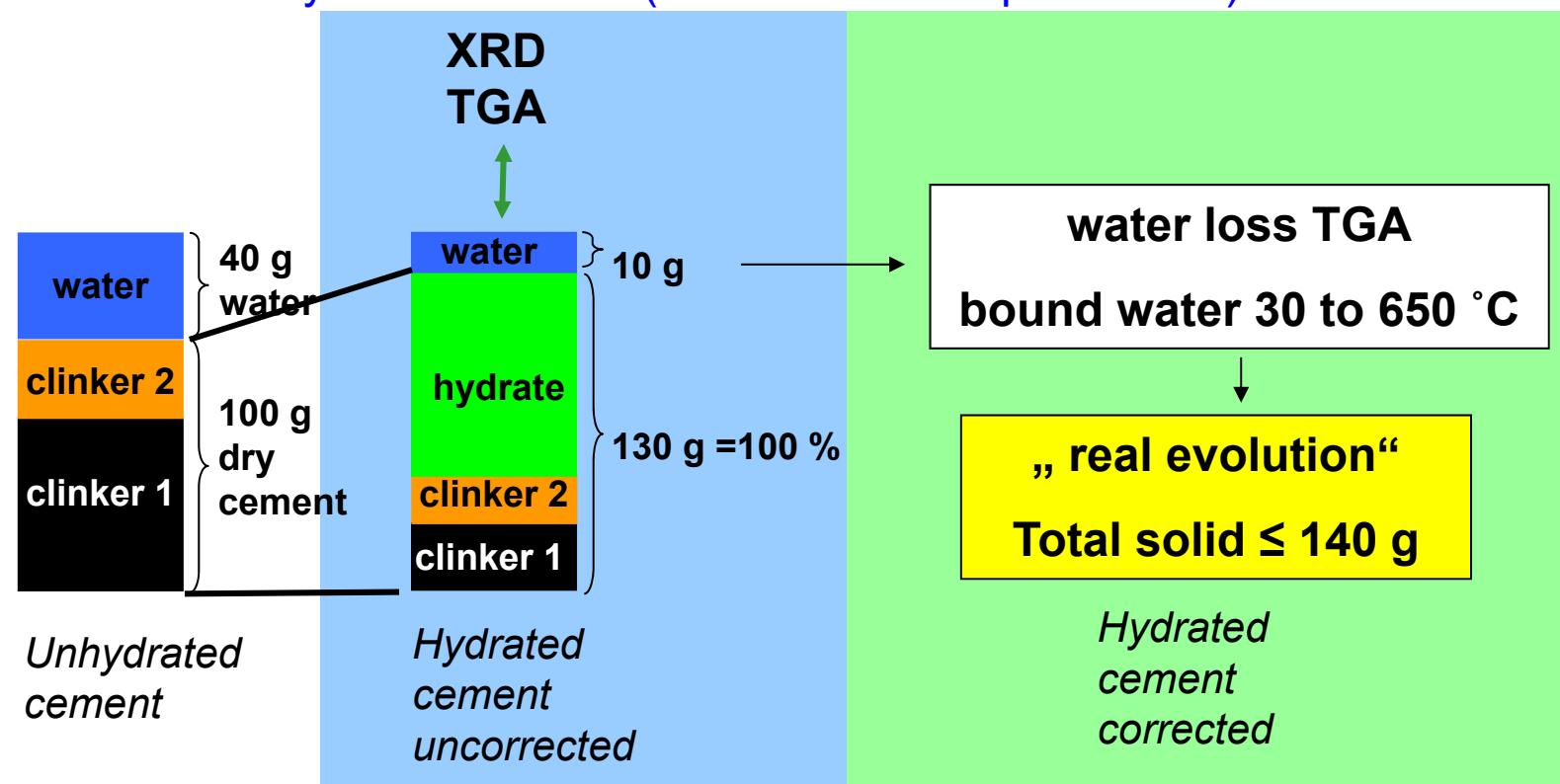
Same input
Modified output
Refers to hydrated cement

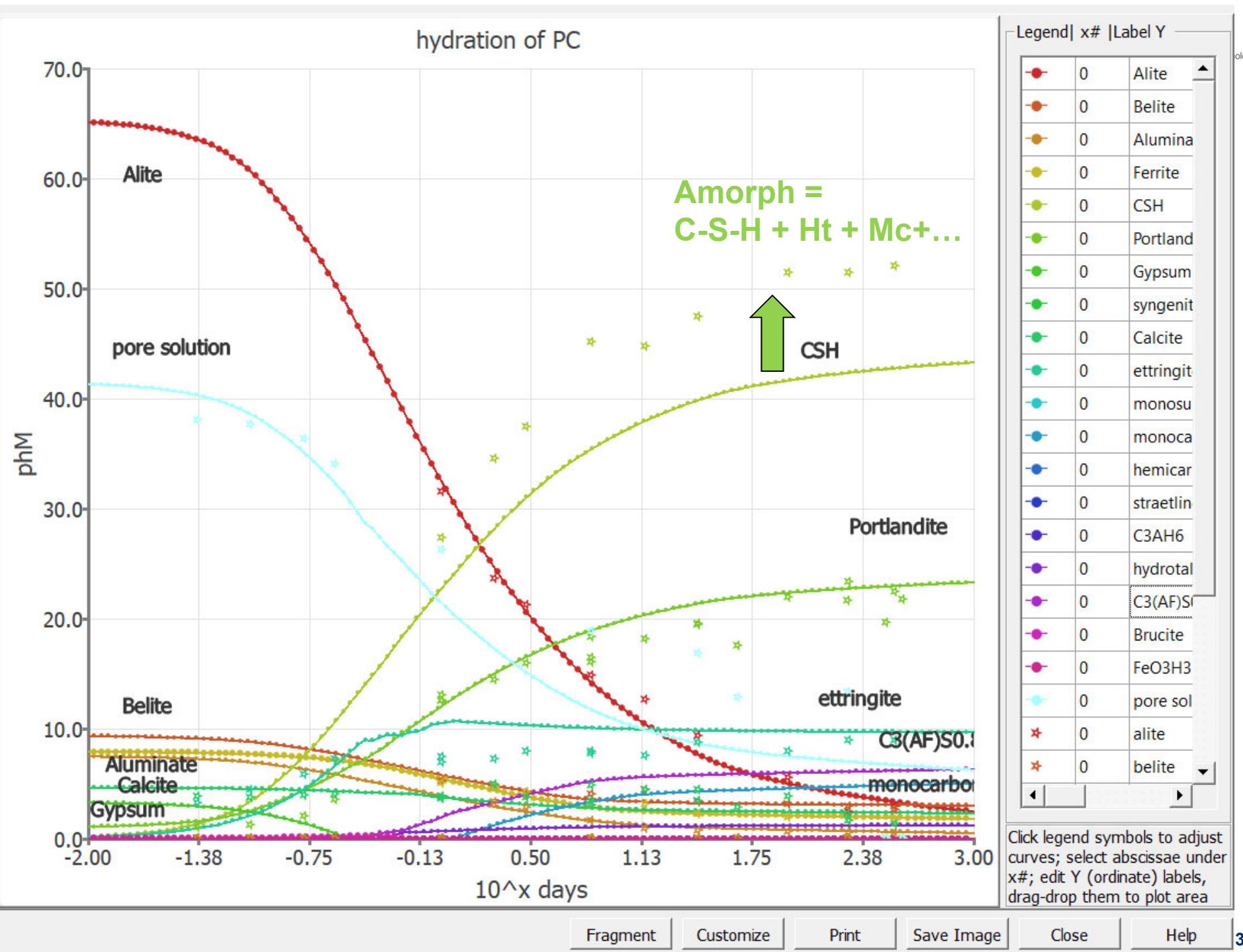
$(1+modC[1][5]-phM[{aq_gen}]/100)$
 $=1+0.4\text{-mass H}_2\text{O unreacted}/100$
 $=\text{mass hydrated cement}$
 $(\text{after removal of pore water})$

For comparison with XRD/TGA

Different outputs possible

- Y-axis Mass in g/100 g of original cement
 $\text{phM}\{\text{Portlandite}\}$ => correct measurements to 100 dry weight
- Y-axis Mass in g/100 g of hydrated cement
 $\text{phM}\{\text{Portlandite}\}/(1+\text{modC}[1][5]-\text{phM}\{\text{aq_gen}\})/100)$
correction of the output $/(1+0.4\text{-mass H}_2\text{O unreacted}/100)$
=> / mass hydrated cement (after removal of pore water)

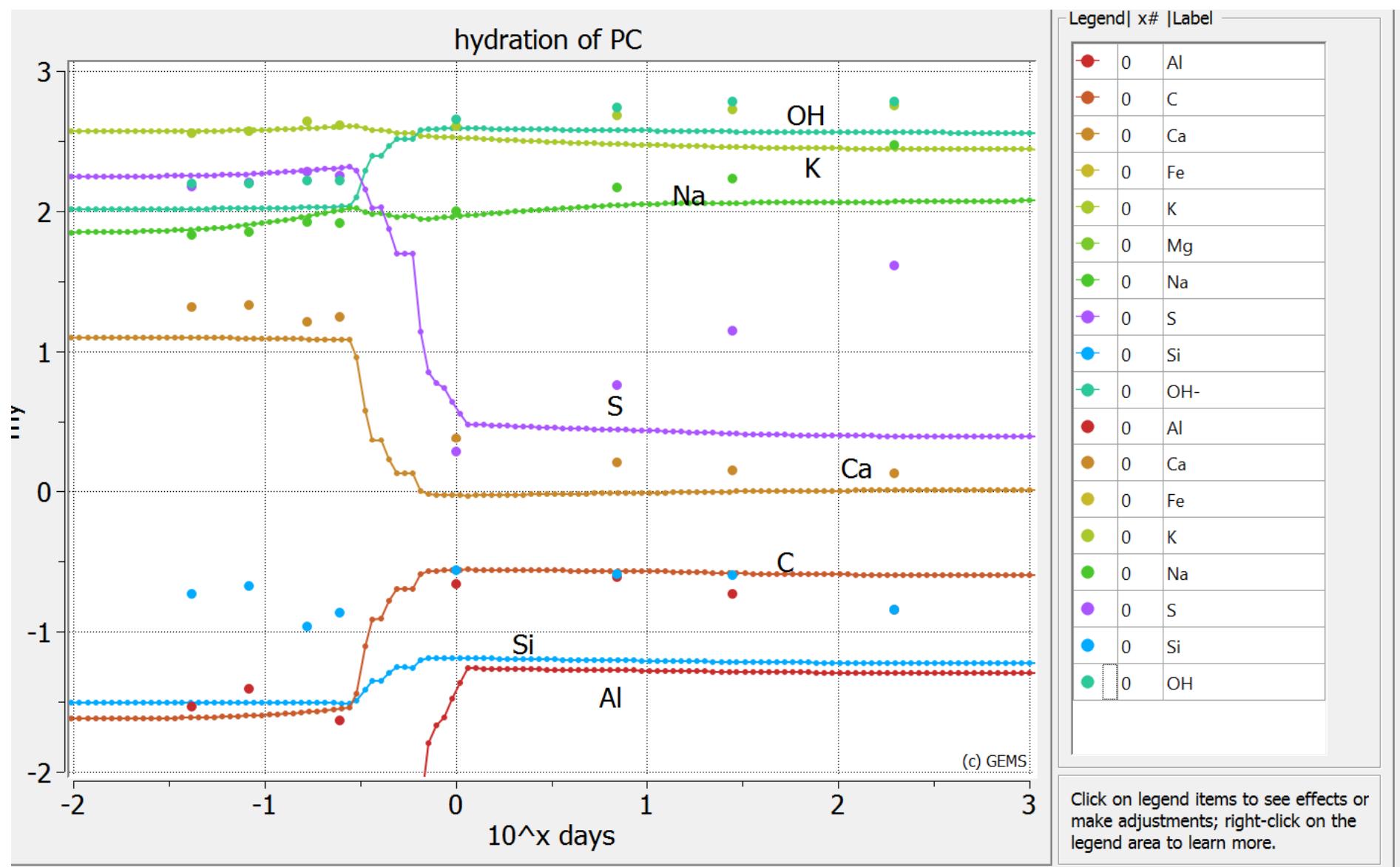




Sampling of aqueous concentrations

- Controls (= input) identical
- Page sampling and results adapted

Controls	Sampling	Results	Config	11/05/2017, 12:57						
NeIt	9999	129	Next	1	I	0	J	128	Jp	128
pSTkey hydration:G:PC:0:0:1:20:0:								cTm	1128	
cTau	0	cpXi	0	cXi	1	cNu				
cpH	0	cpe	0	cEh	0	cT				
<pre>\$ Abscissa xp[J] := lg(modC[J][0]); \$ Ordinates (in mmol/l l solution) transformation molal -> molar yp[J][0] := lg(m_t{Al}*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][1] := lg(m_t[{C}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][2] := lg(m_t[{Ca}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][3] := lg(m_t[{Fe}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][4] := lg(m_t[{K}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][5] := lg(m_t[{Mg}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][6] := lg(m_t[{Na}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][7] := lg(m_t[{S}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][8] := lg(m_t[{Si}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000); yp[J][9] := lg(my[{OH-}]*x[{H2O@}]*18.0153/phVol[{aq_gen}]*1000);</pre>										



Common exercise

- Calculate volumes of the hydrating cement
- Hint:
 - Duplicate process «mass»
 - Exchange phM by phVol (use «word» to do that)
 - Equivalent expression:
 $/mmDC[\{C3S\}]*vol[\{C3S\}]$
„mmDC[{}]" Mass of component
„vol[{}]" Volume of component

