

What's sour and what's sweet in modelling and validating metal processing

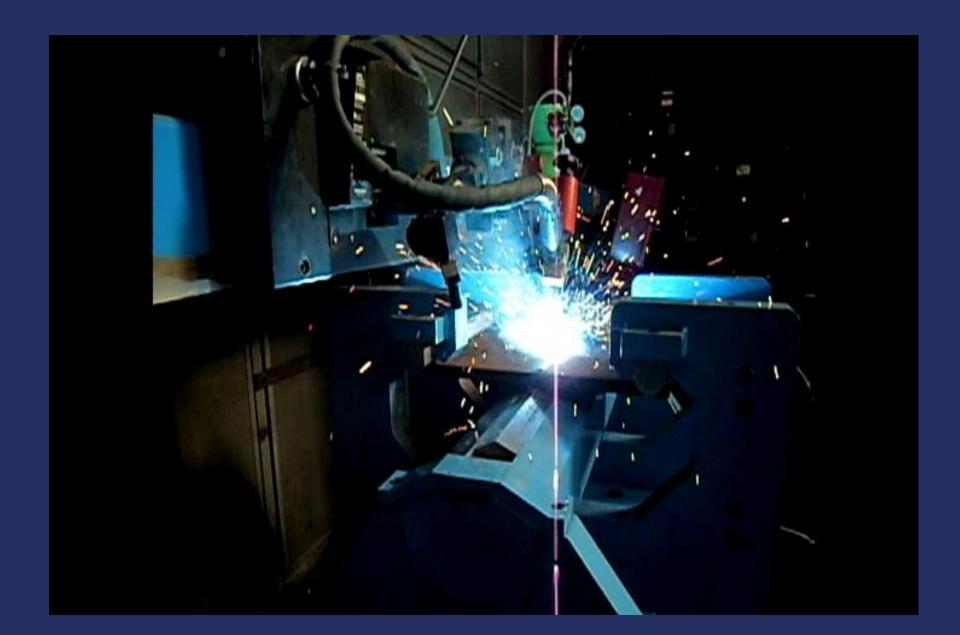
Hongbiao Dong (Hong) *University of Leicester, UK*

Third International workshop on validation of computational mechanics models,

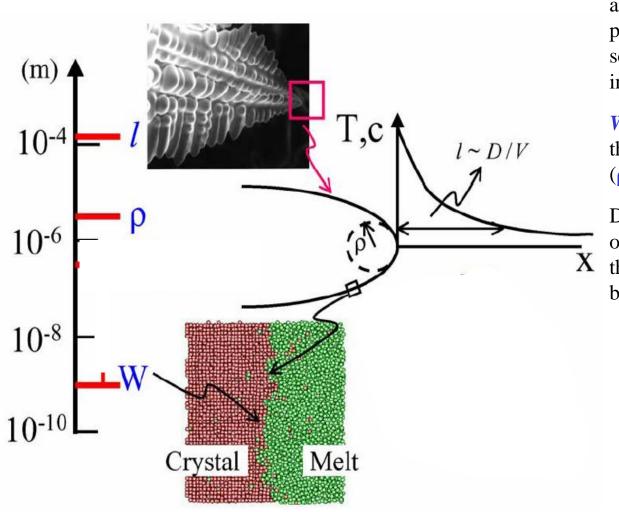
12th June, 2014 at the Neus Rathaus, Munchen



Welding Process



Multi-scale challenge of metal processing (solidification and its application in casting and welding)

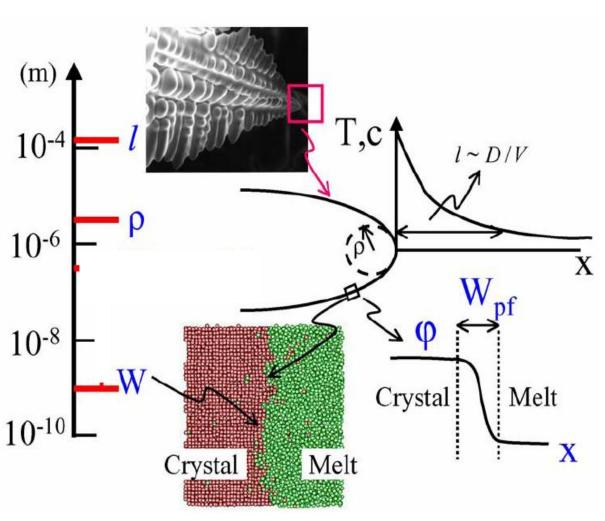


energetic and kinetic properties of S/L are determined by atomic scale processes acting over the nano-meter scale with width *W* of the real S/L interface.

W is three-orders of magnitude smaller than the curvature of the dendritic tip (p),

Dendritic tip radius (ρ) is one or two orders of magnitude smaller than the thickness of the solute diffusion boundary layer (l).

Multi-scale challenge of metal processing (solidification and its application in casting and welding)

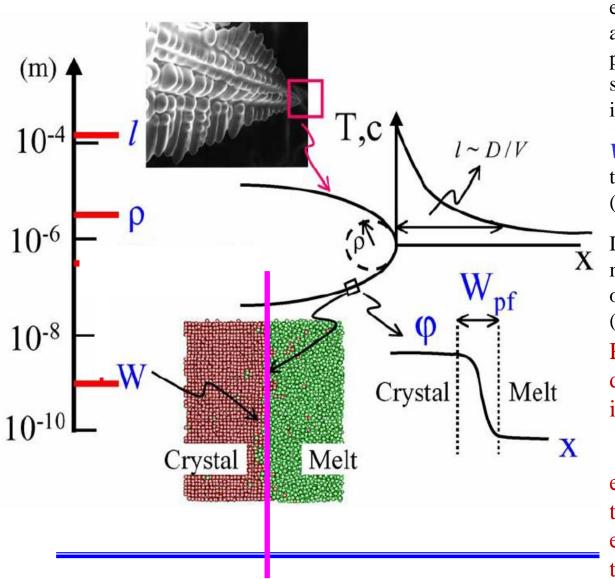


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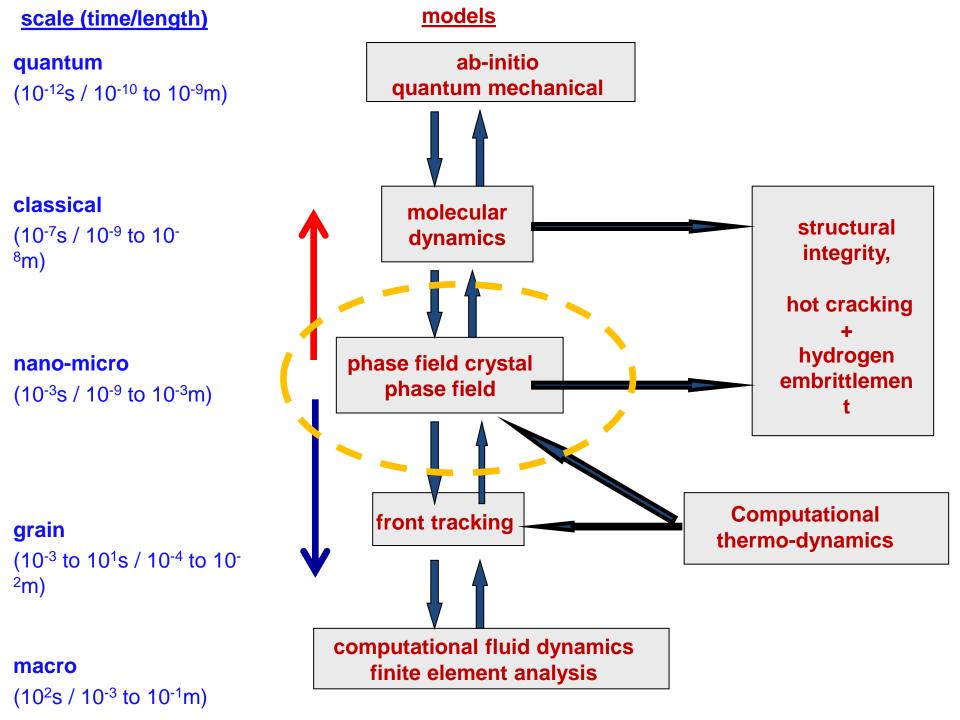
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Phase field simulations of dendritic growth use a microscopic interface width (W_{PF}) .

 $W_{PF} >> W$ and is just small enough to resolve the curvature of the advancing crystals, but large enough to render the computations tractable.



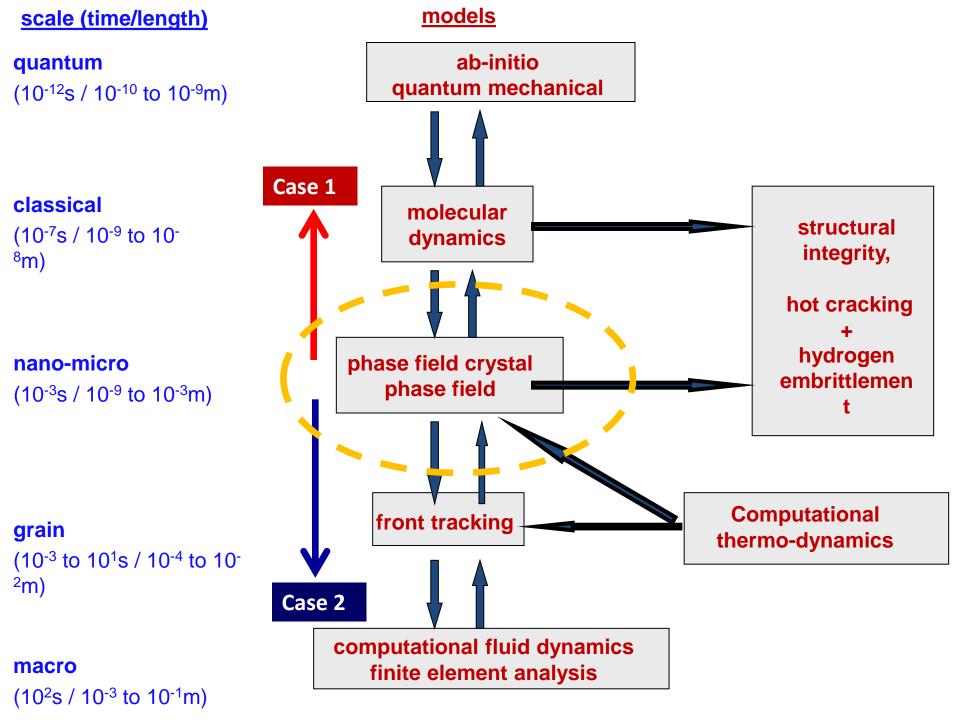


Modelling linking and Integration: EU FP7 Project in Multi-scale Modelling of Welding

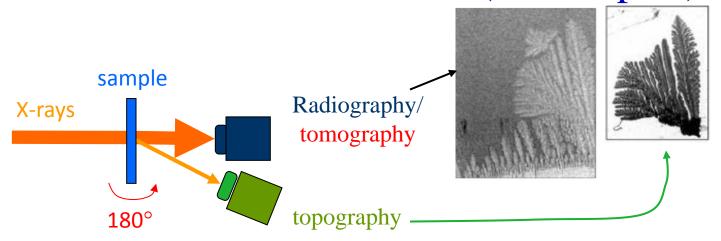
Mint We COOPERATION

U. Leicester, UK
UCD, Ireland
U. Oxford, UK
TUDelft, Netherlands

KTH , Sweden NTNU, Norway TWI, UK Tata Steel ISPL, Poland FRENZAK, Poland EPFL, Switzerland



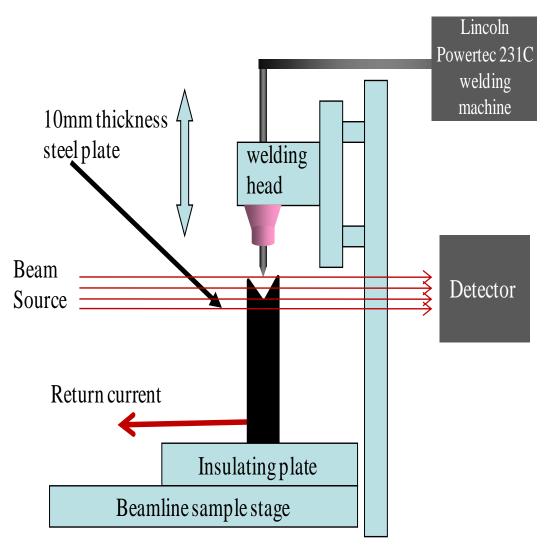
Phenonmena can be validated (2 examples)



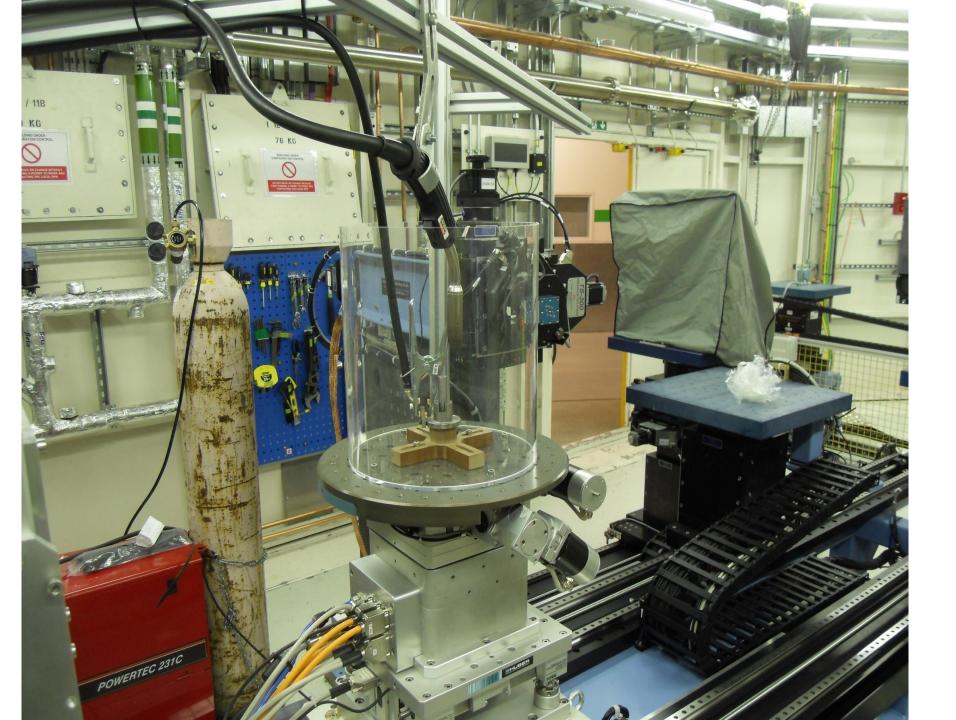
- In-situ SR radiography (1998 NTNU (**ESRF**))
 - 2D, direct, $\Delta r_n \sim 1.2 \ \mu m/ \ \Delta t_e \sim 0.1 \ s$, good dynamic absorption/refraction contrast, alloys
 - s/l-interface, solute boundary, hydrodynamics
 - 2008: Performed by > 12 groups world wide
- Ultra-fast in-situ SR tomography (2004 INPG (**ESRF**))
- 3D indirect, $\Delta r_n \sim 3 \ \mu m / \ \Delta t_e \sim 10 \ s$, absorption/refraction contrast, alloys, $f_s > 0.3$
- s/l-interface, final stages of solidification (hot tears, porosity, precipitates)

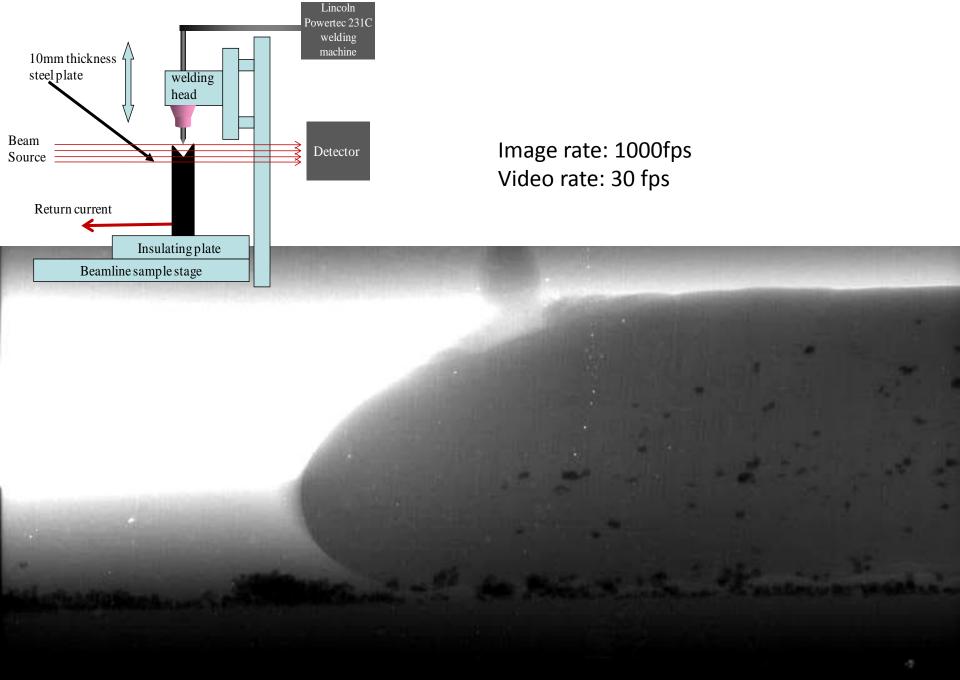
X-ray imaging techniques

An industrial-scale arc-welding setup

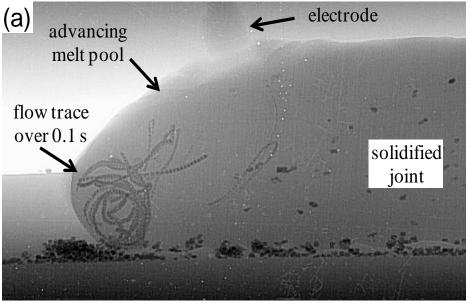


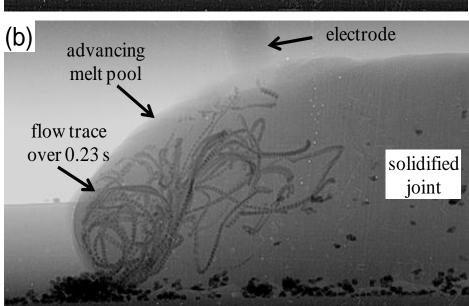
remotely controlled metal active gas (MAG)

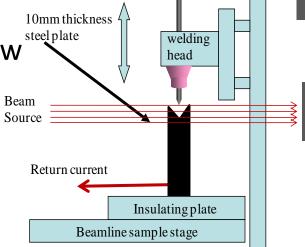




single streamlines of flow





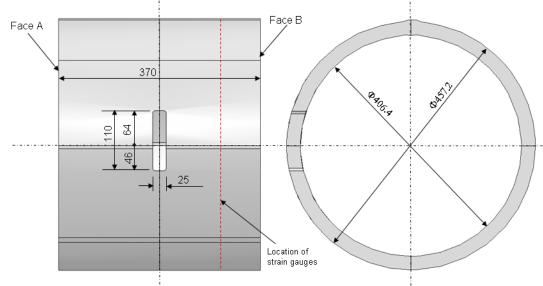


(a) over 50 mini seconds

(b) over 120 mini seconds(X-ray radiography)

Phenonmena can be validated (2nd examples)

Neutron diffraction residual stress measurement: UOE pipe

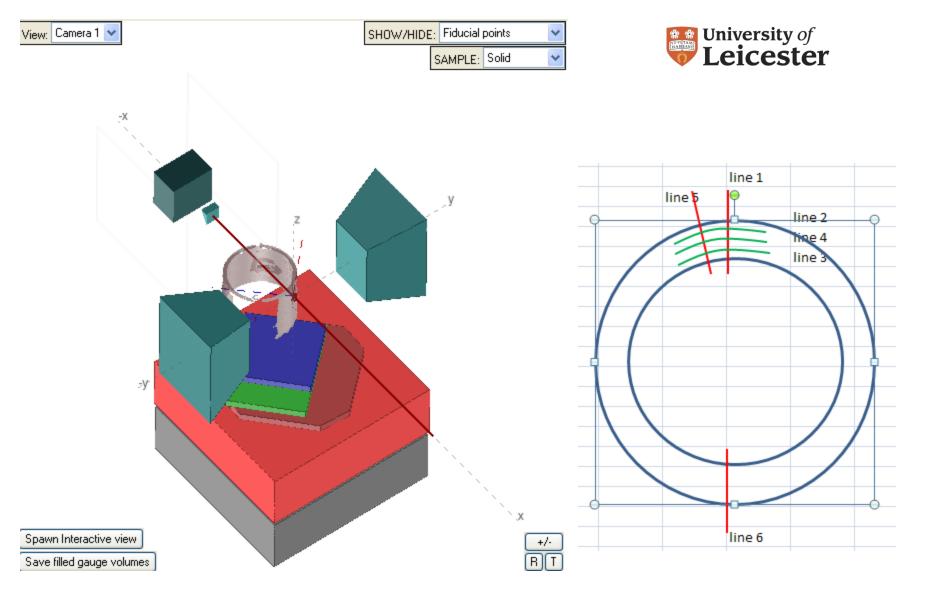


Pipe sample design & preparation

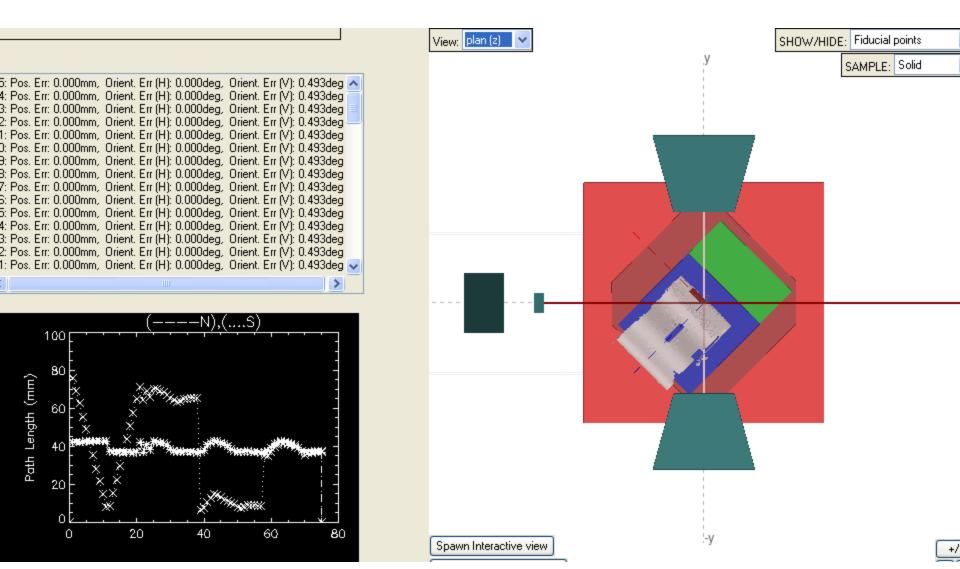


Actual pipe sample with fiducial points

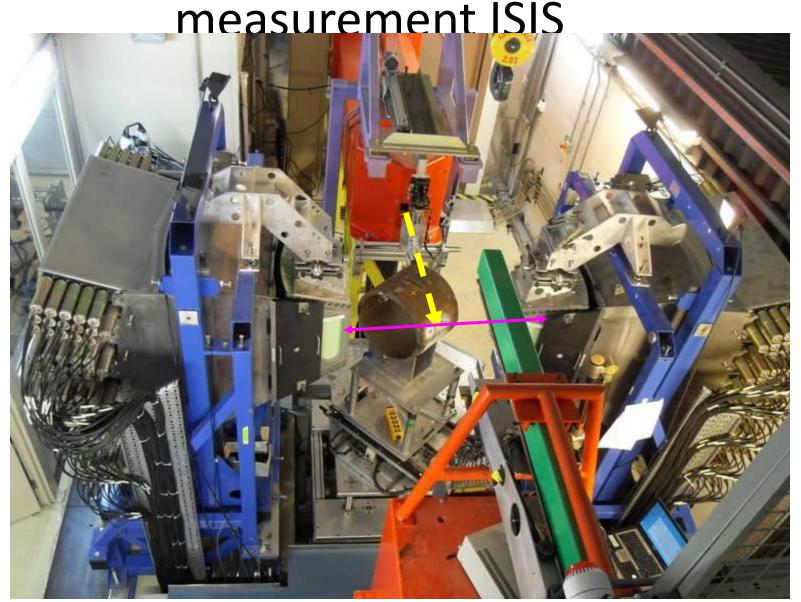
Specimen design & preparation for D₀ scanning





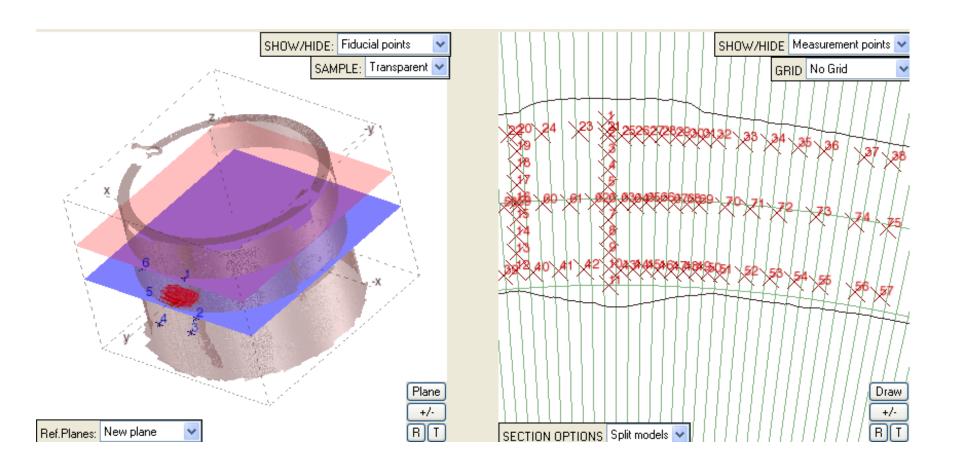


Neutron diffraction residual stress

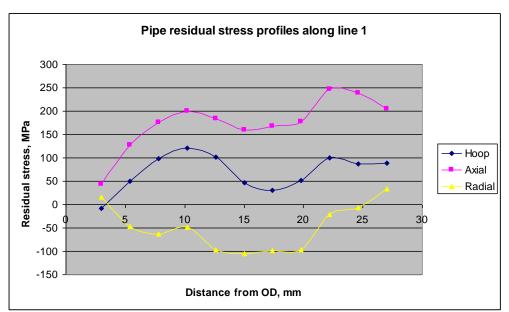


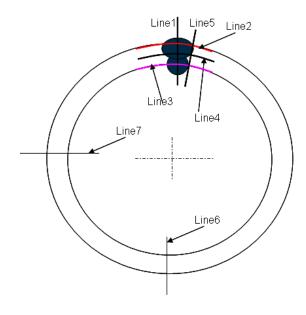


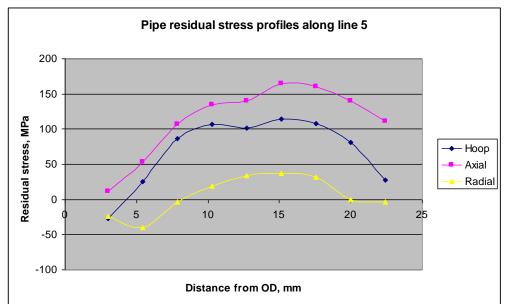




Neutron diffraction residual stress measurement: preliminary results



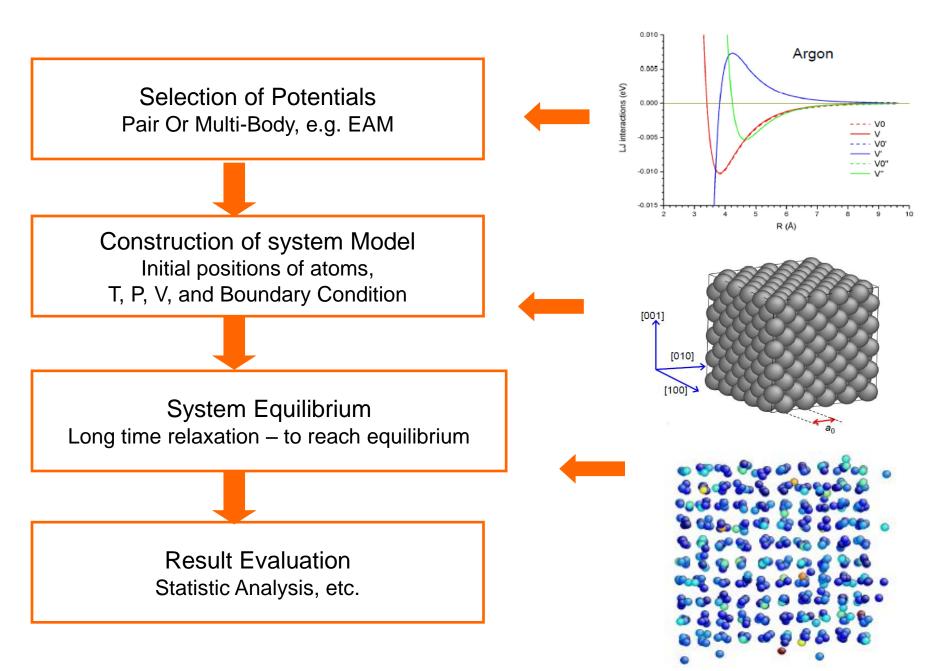




Data is difficult to be validated (prediction) from Molecular Dynamics Simulation

- ➤ Thermodynamic and kinetic Data (Fe)
 - ➤ Melting Temperature
 - ➤ Density
 - Enthalpy, latent heat and specific heat
 - > Diffusion coefficient
 - ➤ Solid-liquid interfacial energy and its anisotropy
 - >Anisotropy of kinetic coefficient

MD Simulation Procedure



EAM Potentials for BCC Fe

H(x): Heaviside function

• Pair potential:

$$\phi(r) = \sum_{k} a_{k} (r - r_{k})^{n_{k}} \underbrace{H(r_{k} - r)} H(r - r_{2})$$

$$+ H(r_{2} - r) H(r - r_{1}) \exp(B_{0} + B_{1}r + B_{2}r^{2} + B_{3}r^{3})$$

$$+ H(r_{1} - r) \underbrace{Q_{i}Q_{j}}_{r} \xi(r/r_{s})$$
nuclear charges

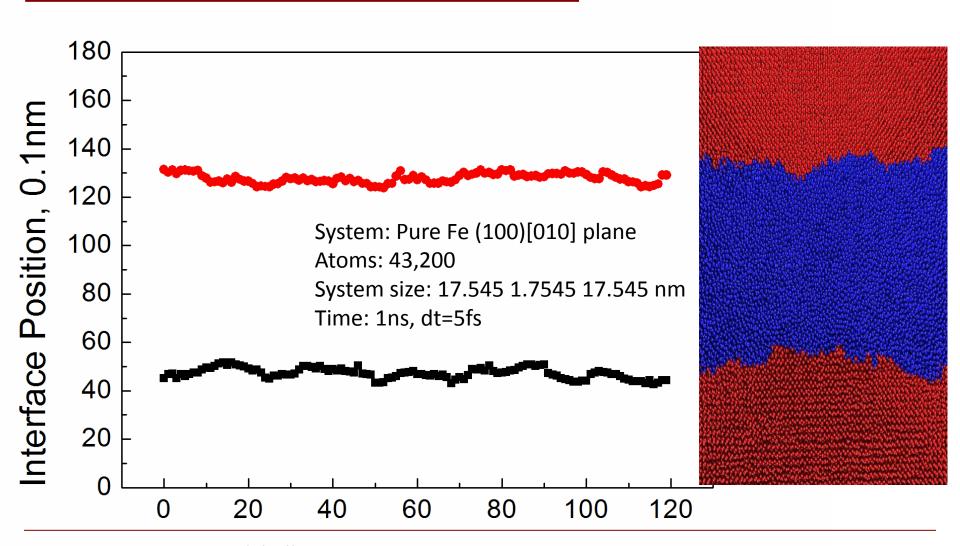
• Density function:

$$f(r) = \sum_{K} A_{k} (R_{K} - r)^{3} H(R_{K} - r)$$

• Embedded function:

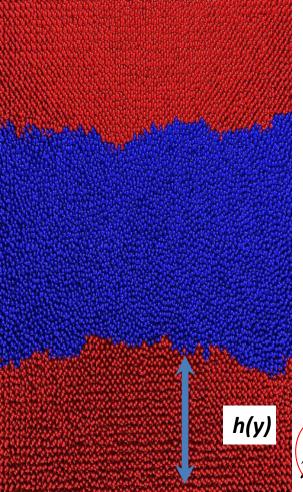
$$F(\rho) = -\sqrt{\rho} + a_2 x^2 + a_4 x^4$$

Solid-liquid interface fluctuation



Liu, Dong, Davidchalk, Com. Mat. Sci. 2013

Interface anisotropy - Capillary fluctuation method



Relationship between interface fluctuations and γ

$$\widetilde{\gamma}(\theta) = \gamma(\theta) + \frac{d^2 \gamma}{d\theta^2}$$
 interface stiffness

Interface free energy

$$\gamma(n)/\gamma_0 = 1 + \varepsilon_1 \left(\sum_{i=1}^3 n_i^4 - \frac{3}{5} \right) + \varepsilon_2 \left(3 \sum_{i=1}^3 n_i^4 + 66 n_1^2 n_2^2 n_3^2 - \frac{17}{7} \right)$$

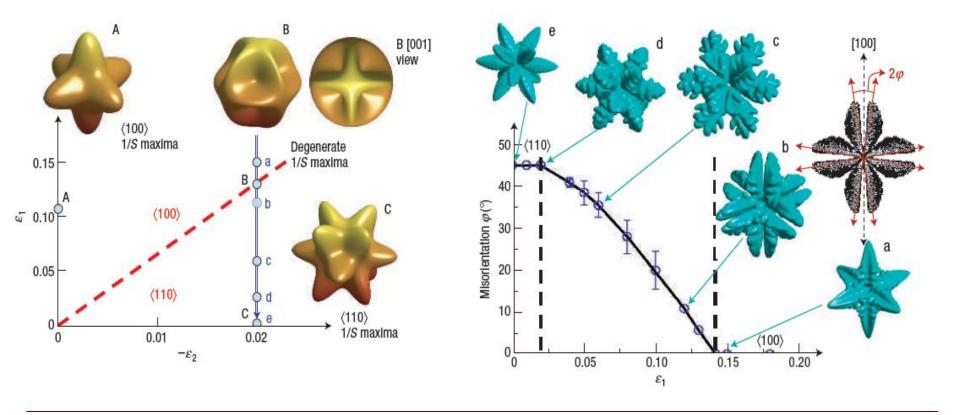
Anisotropy of interface energy

Potential:	ABCH*	Pair*	MH(SA) ^{2*}	This work
Structure:	BCC	BCC	BCC	BCC
$\gamma_0 (\text{mJ/m}^2)$	206(10)	221(14)	175(11)	163.4
$\mathcal{E}_{1}\left(\% ight)$	1.6 ± 0.12	1.3 ± 0.18	3.3 ± 0.18	2.88
$\mathcal{E}_{2}\left(\% ight)$	-0.04 ± 0.28	0.26 ± 0.28	0.24 ± 0.32	-0.0612
$\gamma_{100} (\mathrm{mJ/m}^2)$	207	222	178	165
$\gamma_{110} (\mathrm{mJ/m}^2)$	206	220	174	163
$\gamma_{111} (\mathrm{mJ/m}^2)$	205	221	174	162
$\frac{\gamma_{100} - \gamma_{110}}{2\gamma_0}$ (%)	0.4 ± 0.4	0.5 ± 0.5	1.0 ± 0.6	0.7
$\frac{\gamma_{100} - \gamma_{111}}{2\gamma_0}$ (%)	0.5 ± 0.4	0.4 ± 0.6	1.0 ± 0.2	1.0

Liu, Dong, Davidchalk, Com. Mat. Sci. 2013, *D.Y.Sun, M.Asta, Phys.Rev.B, 69, 174103 (2004)

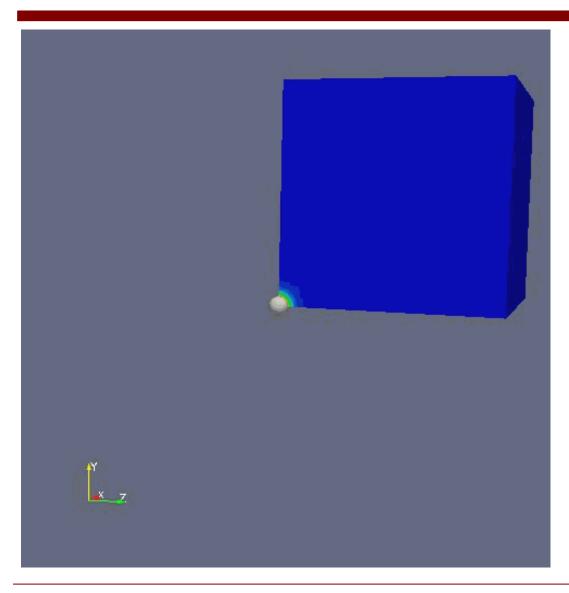
Influence of Interface anisotropy

$$\gamma(\theta, \varphi) = \gamma_0 \left[1 + \varepsilon_1 K_1(\theta, \varphi) + \varepsilon_2 K_2(\theta, \varphi) + \cdots \right]$$



T. Haxhimali, A. Karma, F. Gonzales, M. Rappaz, Nature Mater. Vol 5, 2006, 660-664

Recent results



Input Parameter from MD:

$$\gamma_0 = 163.4 \text{mJ/m}^2$$

$$\varepsilon_1 = 0.0288$$

$$\varepsilon_2 = -0.0006$$

$$T_m = 1900 \text{K}$$

$$L = 0.147 \text{eV}$$

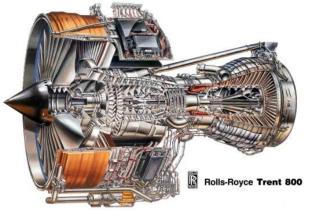
One of most advanced phase field solidification modeling: including

- Adaptive meshing,
- thin interface analysis

Validated against analytical prediction.... Benchmark exercises?

Xie, Dong, Dantzig, Com. Mat. Sci. 2013

models scale (time/length) ab-initio quantum quantum mechanical $(10^{-12}s / 10^{-10} to 10^{-9}m)$ classical molecular structural $(10^{-7}s / 10^{-9} to 10^{-1})$ dynamics integrity, 8m) hot cracking hydrogen nano-micro phase field crystal embrittlemen phase field $(10^{-3}s / 10^{-9} to 10^{-3}m)$ Computational front tracking grain thermo-dynamics $(10^{-3} \text{ to } 10^{1} \text{s} / 10^{-4} \text{ to } 10^{-1})$ ²m) Case 2 computational fluid dynamics macro finite element analysis $(10^2 \text{s} / 10^{-3} \text{ to } 10^{-1} \text{m})$



1540.0

1438.9

1337.8

1236.7

1135.6

1034.4

933.3

832.2

731.1

630.0

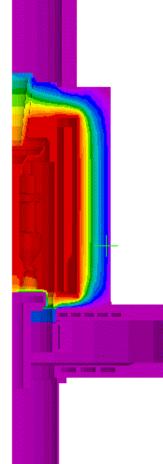
528.9

427.8

326.7

225.5 124.4 23.3

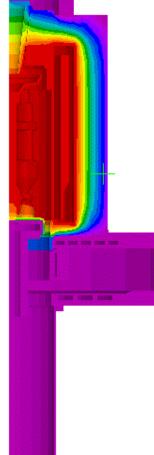
VeriCast Blade







1360.00



1354.00 1348.00 1342.00 1336.00 1330.00 1324.00 1318.00 1312.00 1306.00 1300.00 1294.00 1288.00 1282.00 1276.00 1270.00

Dai, Dong, et al Met Tran A, 2011

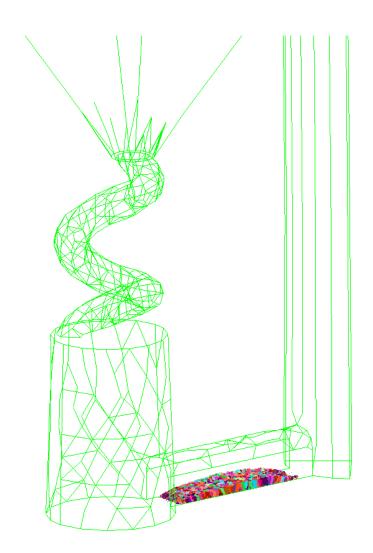
Grain Structure Evolution



Mixed Colours

BBC TV program
April 2012
How metal works?

Dai, Dong, et al Met Tran A, 2011
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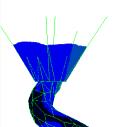


Grain Structure Evolution



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Stochastic Study

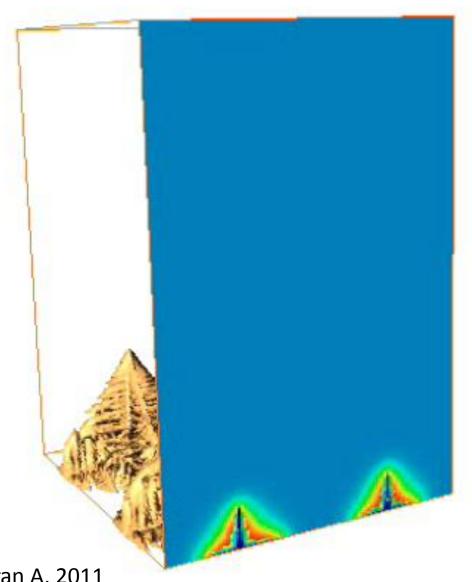






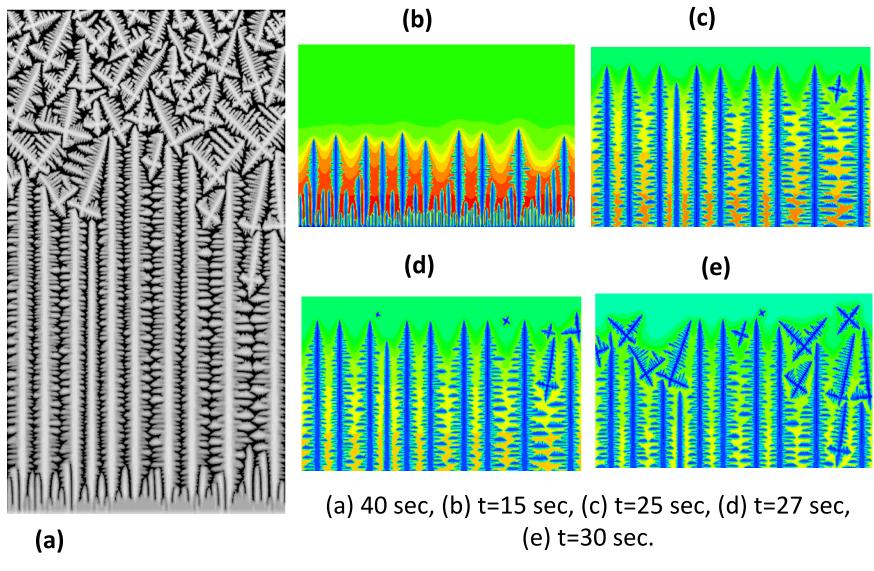
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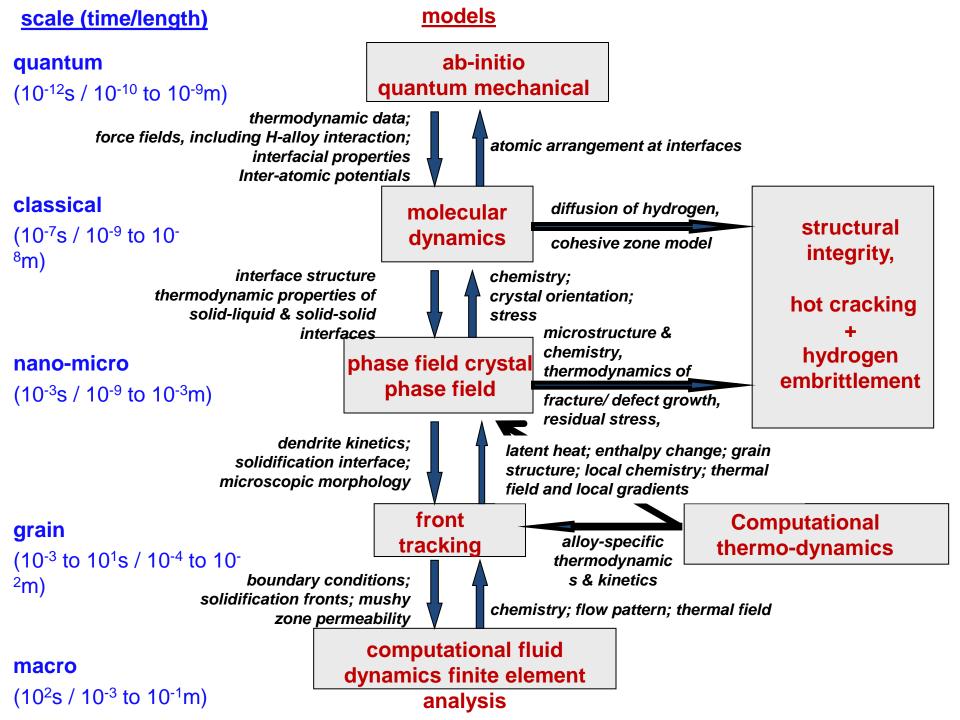


ai, Dong, et al Met Tran A, 2011

Transverse Section Views in 3D Simulations



Dong, Lee, Acta Mat. 2005





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Factories of Future (FOF): ICT Innovation for manufacturing SMEs

Acknowledgement

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